

Stormwater Division

MEMORANDUM

DATE:

March 12, 2010

TO:

Michael J. Gillis, Virginia Correctional Enterprises Document Management Services

FROM:

Jo Anna Ripley, Stormwater

PO:

270712

RE:

Files Approved for Scanning

General File ID or BMP ID:

WC046

PIN: 1310100020

Subdivision, Tract, Business or Owner

Name (if known):

Williamsburg James City County Schools

Property Description:

Stonehouse Elementary

Site Address:

3651 Rochambeau Drive

(For internal use only)

Box 22

Drawer: 9

Agreements: (in file as of scan date)

N

Book or Doc#:

Page:

Comments

Printed On 05/13/2008 By WOOLRIDGE TECH STORE FOR LOCAL

WC 046 Williamsburg Schools O10010662 DECLARATION OF COVENANTS 131010020 INSPECTION/MAINTENANCE OF DRAINAGE SYSTEM Stonehouse Elem.

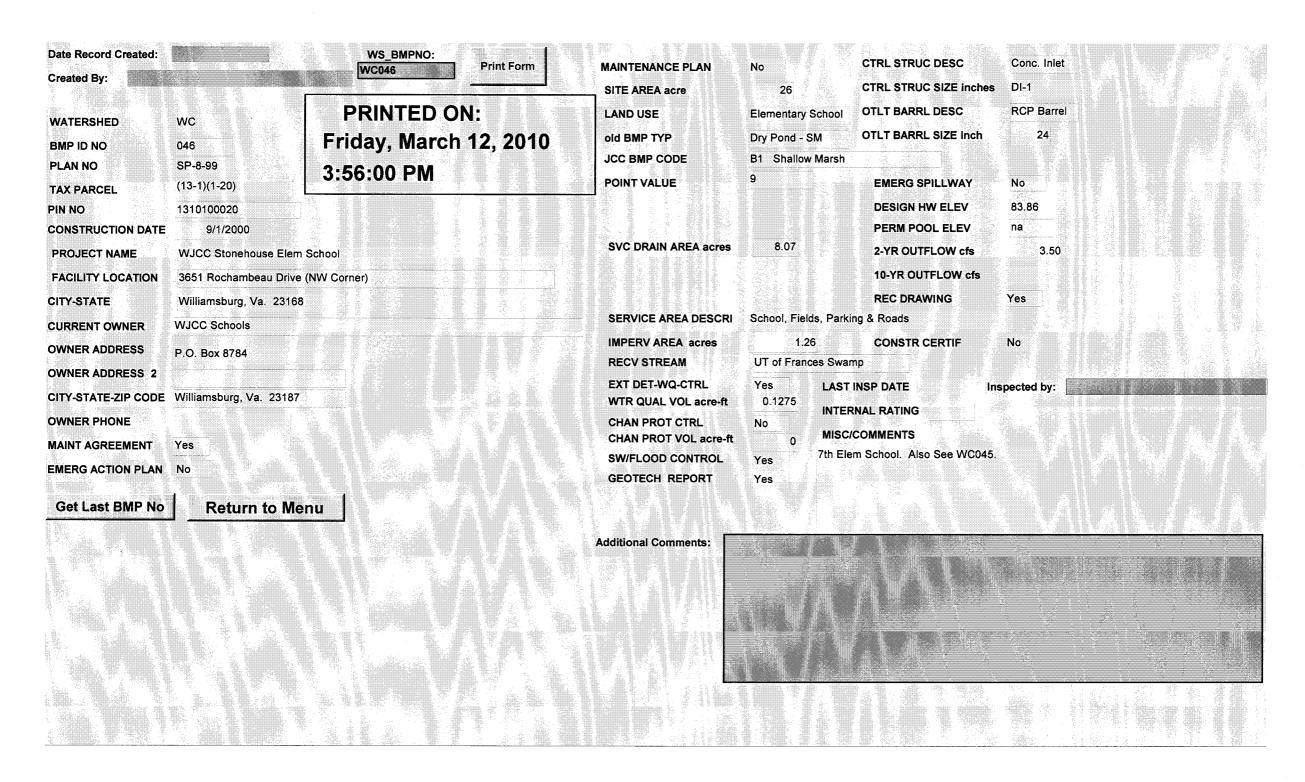
THIS DECLARATION, made this 11th day of June	2001,
between Williamsburg-James City County Public Schools	
and all successors in interest, hereinafter referred to as the "COVENANTOR(S)," owner(following property: 3651 Rochambeau Drive	s) of the
Deed Book P.B. 70, Page No. 34 or Instrument No. 980 015630	
and James City County, Virginia, hereinafter referred to as the "COUNTY."	

WITNESSETH:

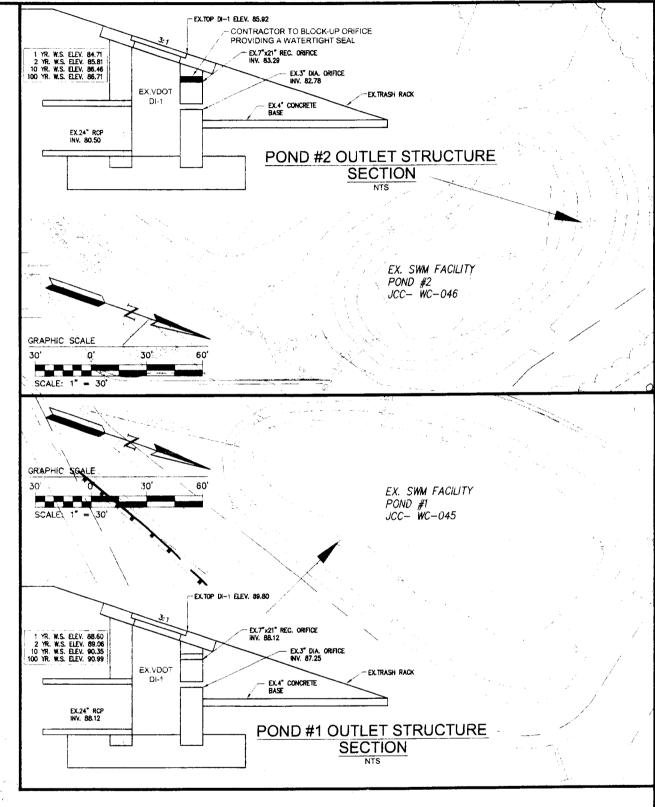
We, the COVENANTOR(S), with full authority to execute deeds, mortgages, other covenants, and all rights, titles and interests in the property described above, do hereby covenant with the COUNTY as follows:

- The COVENANTOR(S) shall provide maintenance for the drainage system including any runoff control facilities, conveyance systems and associated easements, hereinafter referred to as the "SYSTEM," located on and serving the above-described property to ensure that the SYSTEM is and remains in proper working condition in accordance with approved design standards, and with the law and applicable executive regulations. The SYSTEM shall not include any elements located within any Virginia Department of Transportation rights-of-way.
- If necessary, the COVENANTOR(S) shall levy regular or special assessments against all present or subsequent owners of property served by the SYSTEM to ensure that the SYSTEM is properly maintained.
- The COVENANTOR(S) shall provide and maintain perpetual access from public right-of-ways to the SYSTEM for the COUNTY, its agent and its contractor.
- The COVENANTOR(S) shall grant the COUNTY, its agent and its contractor a right of entry to the SYSTEM for the purpose of inspecting, operating, installing, constructing, reconstructing, maintaining or repairing the SYSTEM.
- If, after reasonable notice by the COUNTY, the COVENANTOR(S) shall fail to maintain the SYSTEM in accordance with the approved design standards and with the law and applicable executive regulations, the COUNTY may perform all necessary repair or maintenance work, and the COUNTY may assess the COVENANTOR(S) and/or all property served by the SYSTEM for the cost of the work and any applicable penalties.
- The COVENANTOR(S) shall indemnify and save the COUNTY harmless from any and all claims for damages to persons or property arising from the installation, construction, maintenance, repair, operation or use of the SYSTEM.
- The COVENANTOR(s) shall promptly notify the COUNTY when the COVENANTOR(S) legally transfers any of the COVENANTOR(S)' responsibilities for the SYSTEM. The COVENANTOR(S)' shall supply the COUNTY with a copy of any document of transfer, executed by both parties.
- The covenants contained herein shall run with the land and shall bind the COVENANTOR(S) and the COVENANTOR(S)' heirs, executors, administrators, successors and assignees, and shall bind all present and subsequent owners of property served by the SYSTEM.
 - This COVENANT shall be recorded in the County Land Records.

OVENANTS as of thi	s <u>llth</u> day of <u>June</u> , <u> </u>	2001
		COVENANTOR(S)
		Jane Martin
TTEST:	Print Name/Title	J. David Martin. Ed.D. Division Superintendent
Wilder of the second of the se		COVENANTOR(S)
	Print Name/Title	
TTEST:		
I hereby certify Notary Public of the St	that on thisthat ofate of Virginia, and for the City/Count	y of <u>James City</u> , aforesai
I hereby certify I hereby certify Notary Public of the Stressonally appeared _ astrument to be their IN WITNESS V	that on this 11+14 day of June ate of Virginia, and for the City/Count J. David Martin Act. WHEREOF, I have hereunto set my lead to the count of the city/Count of the city/C	y of <u>James City</u> , aforesai <u>and did acknowledge the aforegoin</u>
I hereby certify Notary Public of the St ersonally appeared _ nstrument to be their	that on this <u>lithday of June</u> ate of Virginia, and for the City/Count J. David Martin Act.	y of <u>James City</u> , aforesain and did acknowledge the aforegoin
I hereby certify I hereby certify Notary Public of the Stressonally appeared _ Instrument to be their IN WITNESS V June	that on this 11+14 day of June ate of Virginia, and for the City/Count J. David Martin Act. WHEREOF, I have hereunto set my lead to the count of the city/Count of the city/C	y of <u>James City</u> , aforesaid and did acknowledge the aforegoing and and official seal this <u>11th</u> day of
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I hereby certify Notary Public of the Stresonally appeared _ IN WITNESS V June My Commissio	that on this	and did acknowledge the aforegoing and and official seal this 11th day of the Notary Public
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I hereby certify Notary Public of the Stressonally appeared _ Instrument to be their IN WITNESS V June My Commissio	that on this	and did acknowledge the aforegoing and and official seal this 11th day of the August August Cenga. Notary Public This Declaration of Covenants prepared by J. David Martin, Ed.D. (Print Name) Division Superintendent
I hereby certify Notary Public of the St personally appeared _ Instrument to be their IN WITNESS V June My Commissio	that on this	This Declaration of Covenants prepared b J. David Martin, Ed.D. (Print Name) Division Superintendent (Title) to We 101-D Mounts Bay Rd. (Address)
I hereby certify Notary Public of the St personally appeared _ instrument to be their IN WITNESS V June	that on this	This Declaration of Covenants prepared by J. David Martin, Ed.D. (Print Name) Division Superintendent (Title)







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NVF CHRISTAN ACADEMY INC.

AX MAP # (13-1)(1-3)

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FELL OWS-APP



5248 Olde Towne Road, Sulie Williamsburg, Virginia 23188 (757) 253-0040 Fax (757) 220-8994



CONSULTING ENGINEERS

AMENDED SITE PLAN TONEHOUSE ELEMENTARY SCHOOL လ် ရွိ CHOOL Ø \circ BL <u>a</u> JCC Rect

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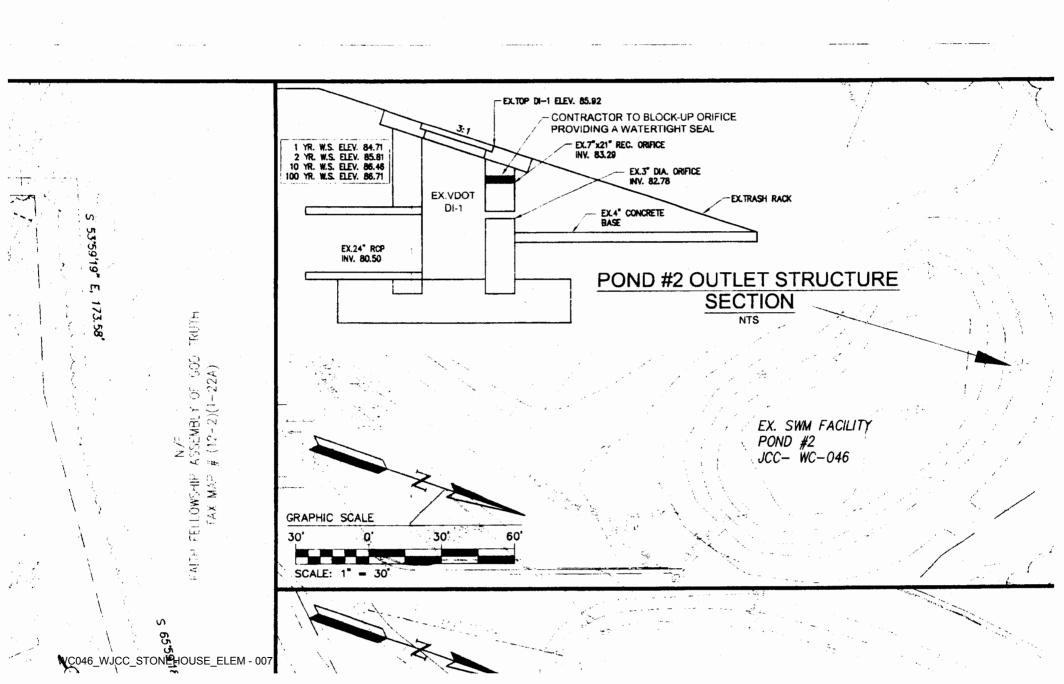
STORMWATER MANAGEMENT/ BMP FACILITY MAINTENANCE PLAN

PROPER MAINTENANCE OF THIS FACILITY IS ENCOURAGED TO PREVENT THE INTRODUCTION OF DEBRIS AND SEDIMENT IN TO THE FACILITY, SPILLWAY AND DOWNSTREAM WATERWAYS. INSPECTIONS FOR SEDIMENT BUILDUPS MUST BE PERFORMED AT LEAST QUARTERLY. IT IS ANTICIPATED THAT UNDER NORMAL CONDITIONS, SEDIMENT REMOVAL FROM THE FACILITY WILL BE REQUIRED ONCE EVERY 10 YEARS IF OTHER CONSTRUCTION OR RELATED ACTIVITIES ARE PERFORMED ON UPSLOPE AREAS, ADEQUATE PROTECTION MUST BE PROVIDED AND INSPECTIONS PERFORMED AT LEAST ONCE WEEKLY UNTIL THE ENTIRE SITE IS STABILIZED.

A DESIGNATED REPRESENTATIVE OF THE DWNER MUST INSPECT THE SWM STRUCTURE AFTER EACH SIGNIFICANT RAINFALL EVENT OR THE FOLLOWING WORKING DAY IF A WEEKEND OR HOLIDAY DCCURS. A SIGNIFICANT RAINFALL FOR THIS STRUCTURE IS DEFINED AS ONE (1) NICH OR MORE OF GAUGED RAINFALL WITHIN A 24 HOUR PERIOD. ONCE PER YEAR, A REPRESENTATIVE OF THE COUNTY MAY JOINTLY INSPECT THE FACILITY. APPROPRIATE ACTION MUST BE TAKEN TO ENSURE PROPER MAINTENANCE.

INSPECTION AND MAINTENANCE OF THE FACILITY WILL CONSIST OF THE FOLLOWING ADDITIONAL MEASURES:

- S 1307'01" W. 348.06 NOTE: TH THE INSPECTION FOR SEDIMENT BUILDUP WITHIN THE FACILITY MUST BE PERFORMED BY VISUAL INSPECTION AND A PHYSICAL DETERMINATION OF SEDIMENT DEPTH WITHIN THE STORAGE AREA. IF THE SEDIMENT REACHES A DEPTH OF 1.0 FT. ABOVE THE DESIGN BOTTOM OF THE FACILITIES, OR IF SEDIMENT THREATENS TO CLOG THE OUTLET STRUCTURE, REMOVAL IS REQUIRED. AT THE SAME TIME, OR AT LEAST ONCE PER YEAR, THE RISER BOTTOM AND OUTLET PIPE MUST BE CLEANED OF ACCUMULATED SEDIMENTS. DISPOSE OF SEDIMENTS REMOVED FROM THE FACILITY AT AN ACCEPTABLE DISPOSE OF SEDIMENTS REMOVED FROM THE FACILITY AT AN ACCEPTABLE
 - 2. PERFORM MAINTENANCE MOMING OF POND GRASSES AT LEAST TIMCE EACH YEAR. GRASSES SUCH AS TALL FESCUE SHOULD BE MOMED IN EARLY SUMMER AFTER EMERGENCE OF THE HEADS ON COOL SEASON GRASSES AND IN LATE FALL TO PREVENT SEEDS OF ANNUAL WEEDS FROM MATURING. MOMING OF LEGUMES CAN BE LESS FREQUENT.
 - 3. PERFORM QUARTERLY INSPECTIONS OF THE RISER SECTION FOR THE OBSERVANCE OF COLLECTED DEBRIS. IMMEDIATELY REMOVE ANY DEBRIS TO MAINTAIN THE INTEGRITY OF THE STRUCTURE AND PROVIDE AN ATTRACTIVE APPEARANCE.
 - 4. PERFORM QUARTERLY INSPECTIONS OF THE SIDE SLOPES OF THE FACILITIES AND DOWNSTREAM WATERWAYS FOR SIGNS OF ANIMAL/RODENT BORROWS OR EROSION. IMMEDIATELY PERFORM NECESSARY REPAIRS, REFLLING OR STABILIZATION AS APPROPRIATE.
 - 5. PERFORM YEARLY STRUCTURAL INSPECTIONS OF THE FACILITY FOR DAMAGE. STRUCTURAL INSPECTION SHALL BE PERFORMED ON THE CONCRETE RISER, TRASH RACK, ORIFICE/ WER(S), OUTLET BARREL AND POND EMBANKMENT. IF DAMAGE IS EVIDENT, REPAIRS MUST BE MADE IMMEDIATELY. DEPENDING ON THE TYPE OF DAMAGE, FURTHER INVESTIGATION BY A PROFESSIONAL ENGINEER MAY BE REQUIRED TO ASSESS THE INTEGRITY OF THE STRUCTURE.



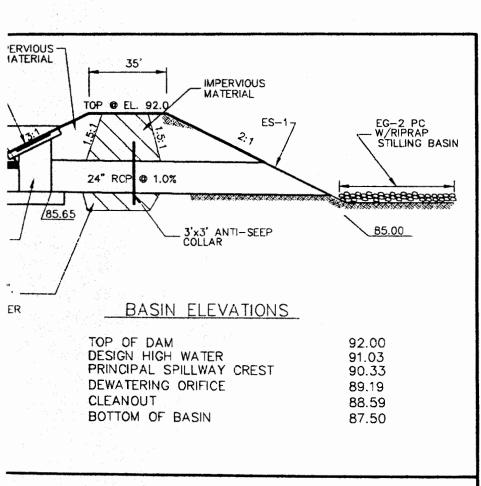
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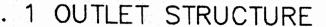
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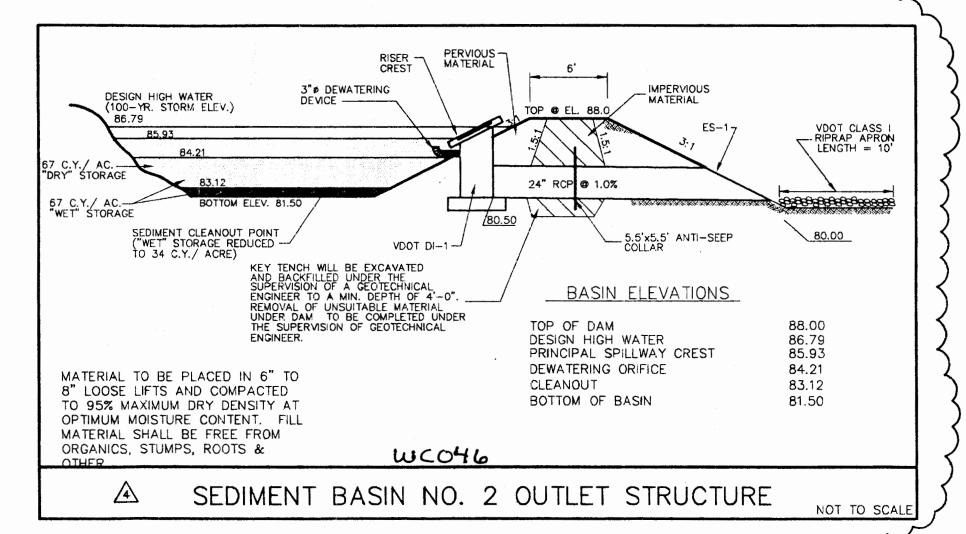
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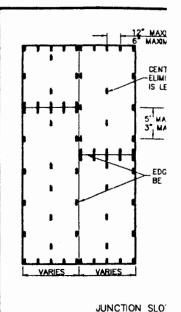
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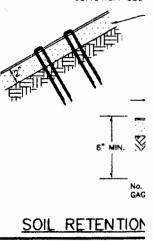




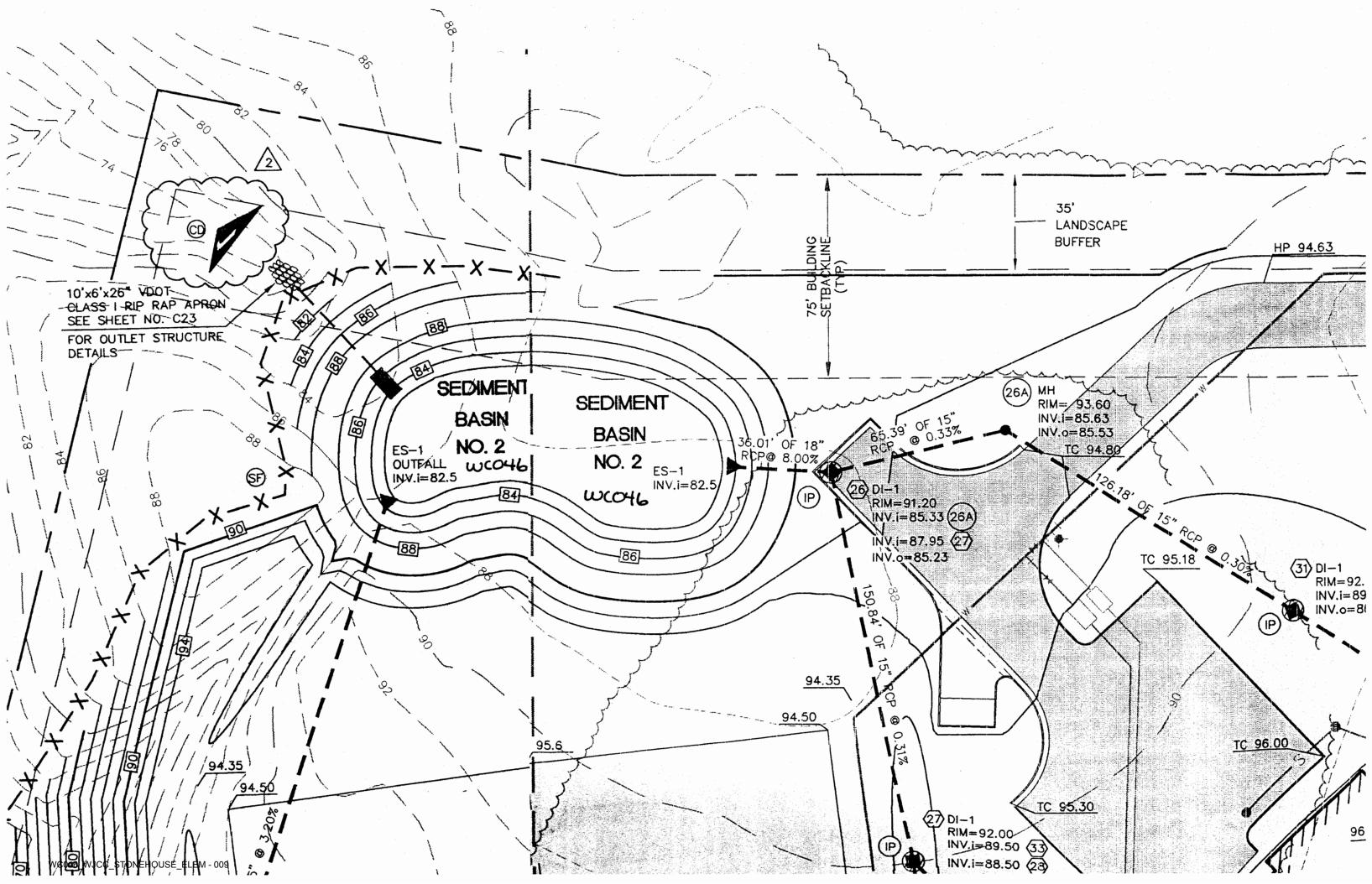
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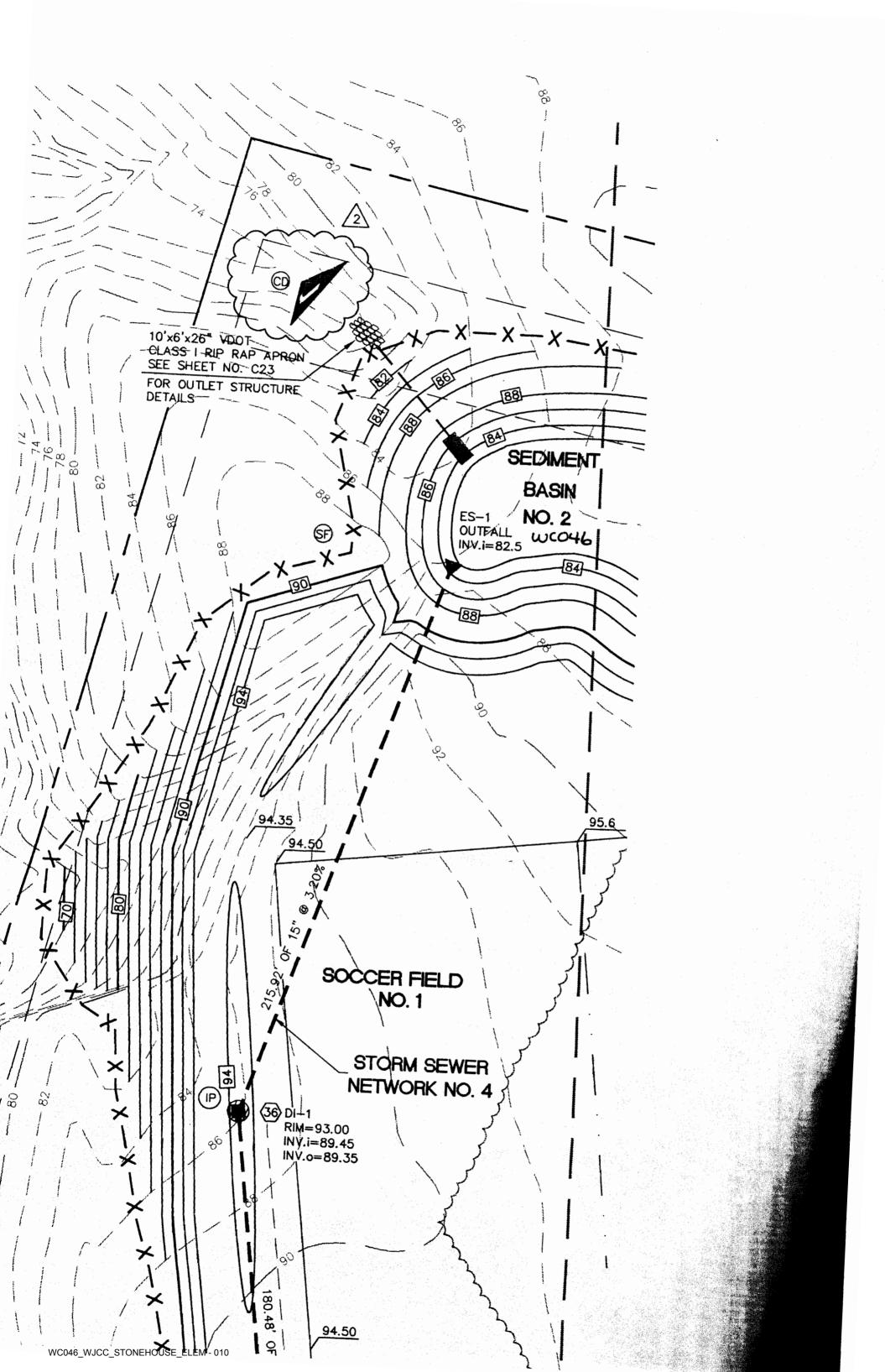


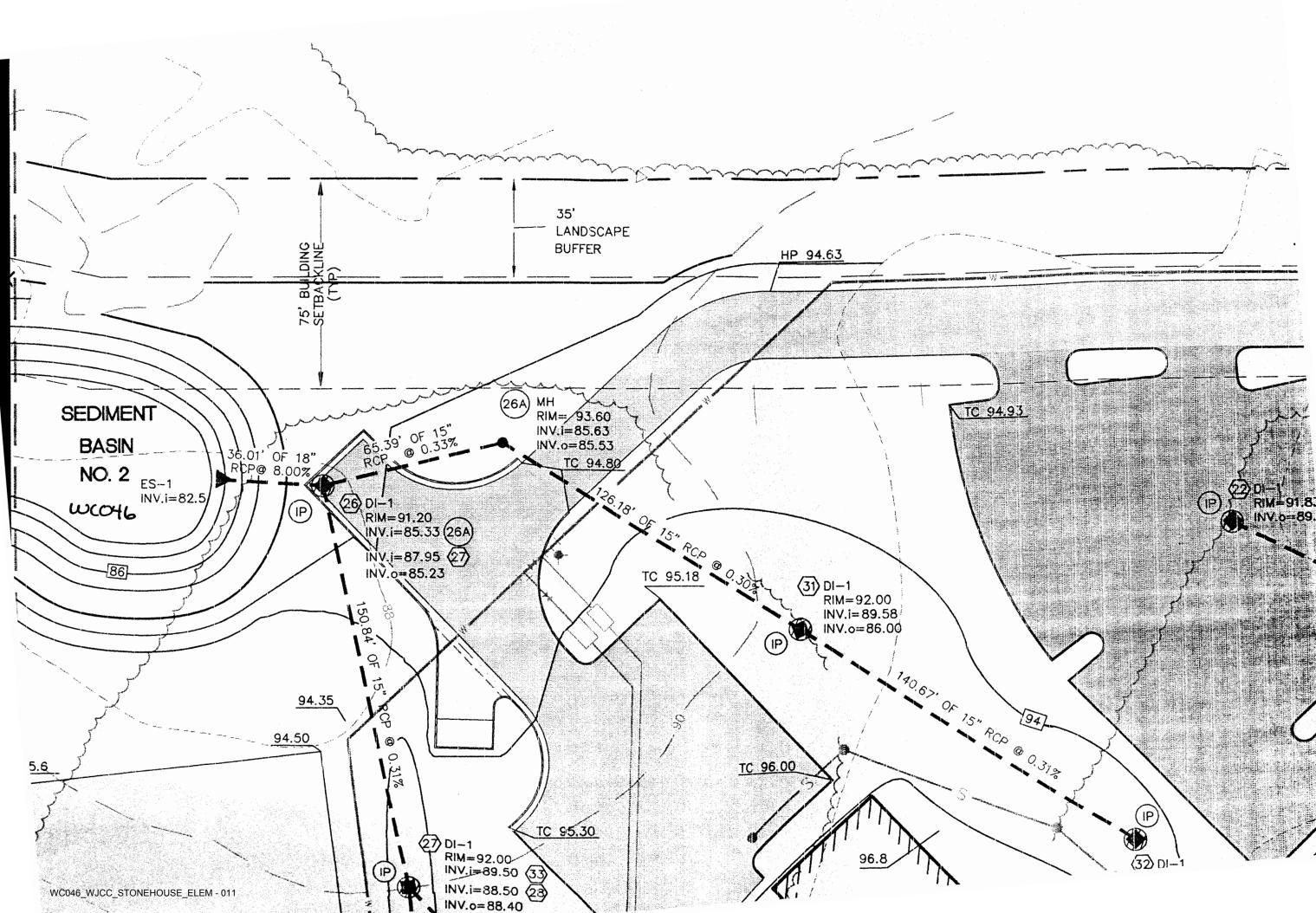


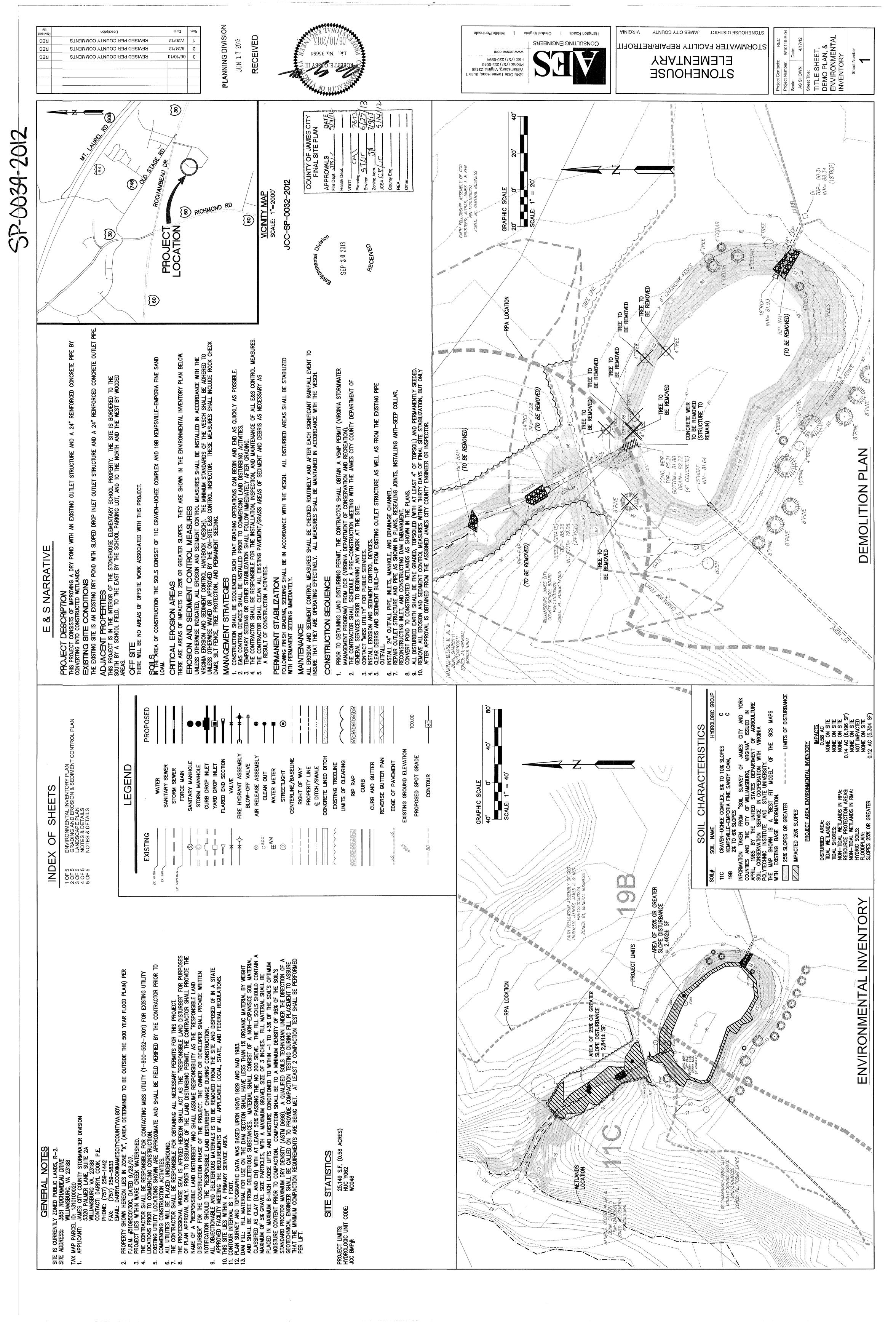


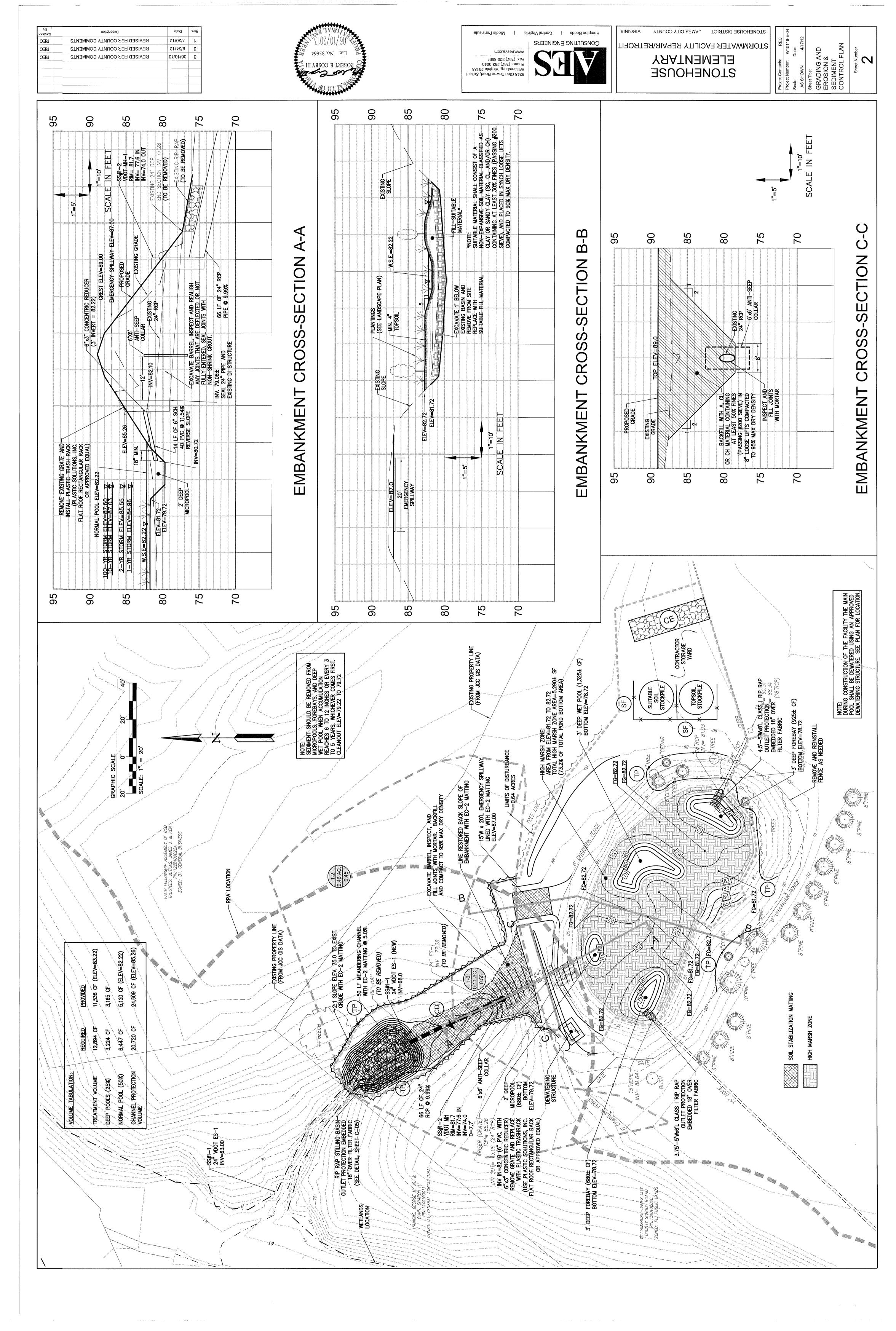
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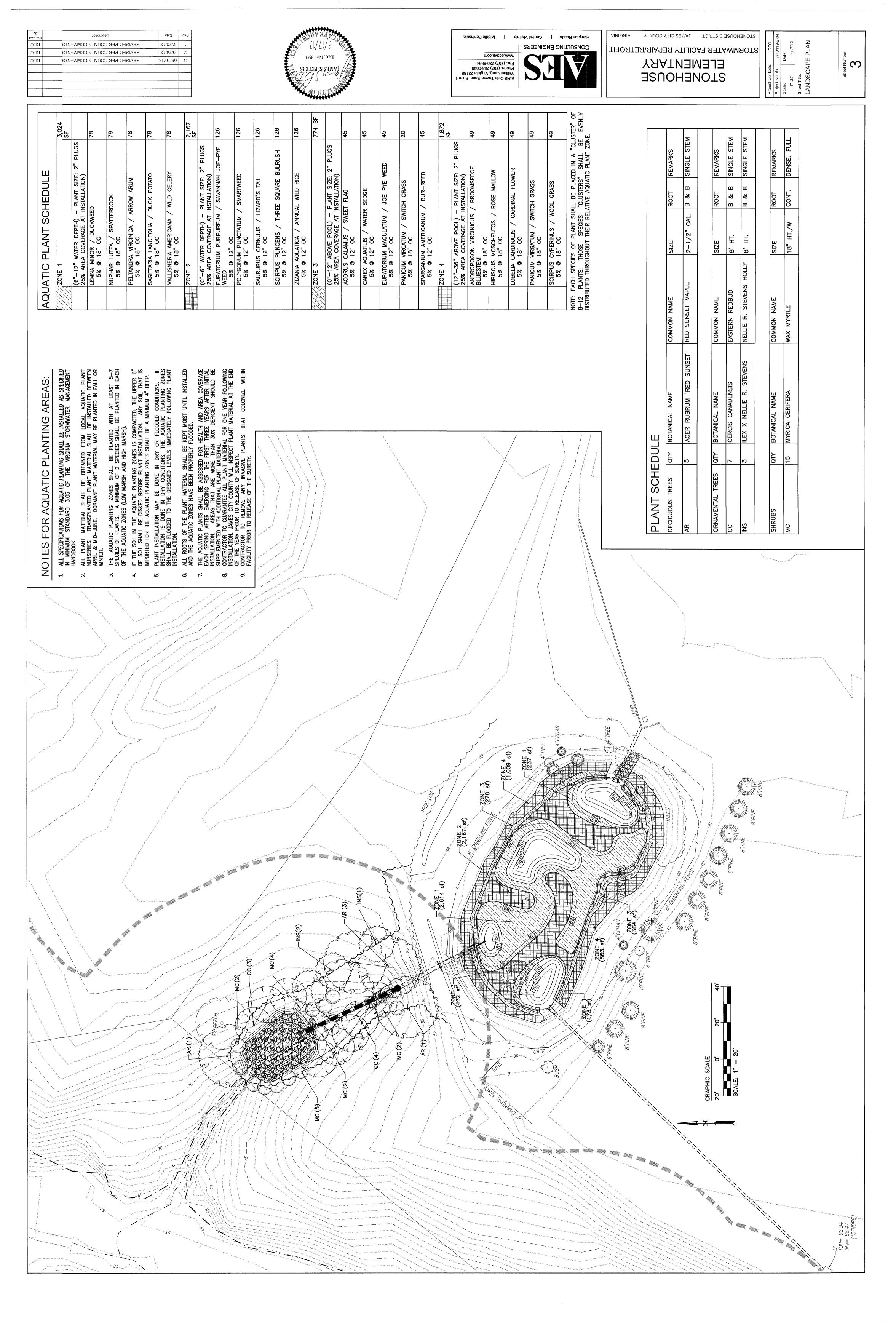


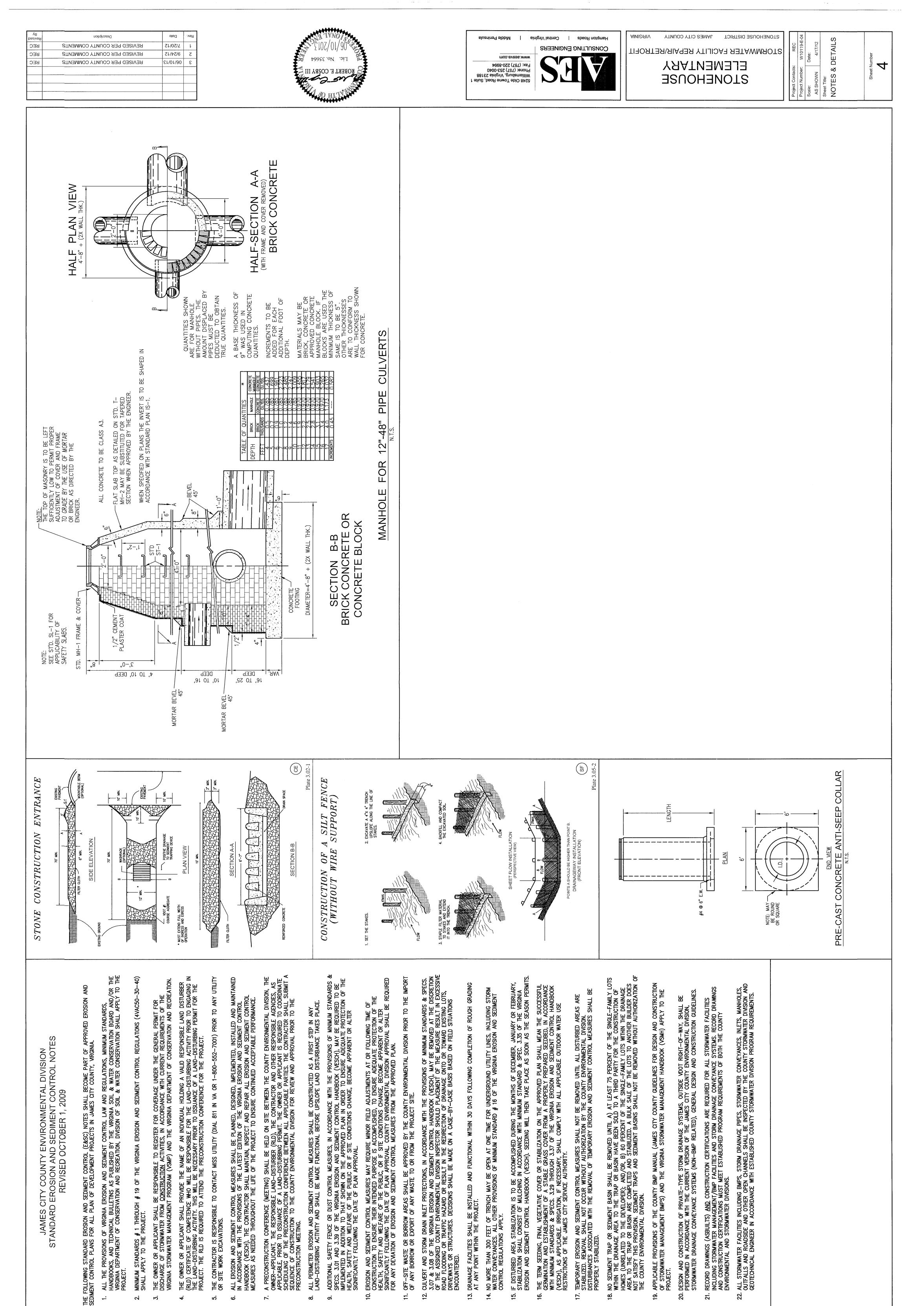












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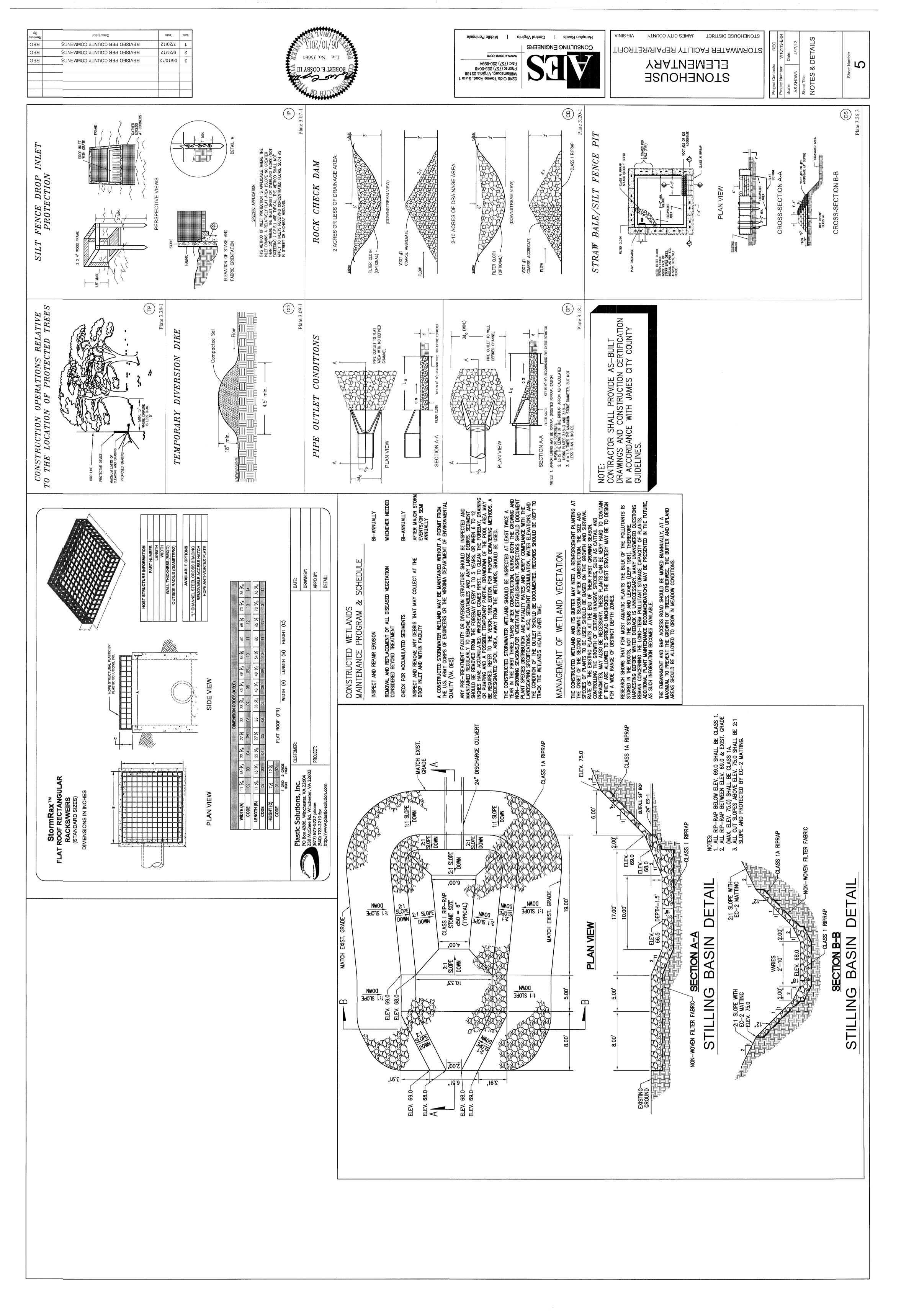
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Stormwater Division

MEMORANDUM

DATE:

July 28, 2014

TO:

Michael J. Gillis, Virginia Correctional Enterprises Document Management Services

FROM:

Jacob Smith, Stormwater Intern

PO:

110426

RE:

Files Approved for Scanning

NAME PDF/SCANNED FILE: STONEHOUSE ELEMENTARY STORMWATER REPAIR AND RETROFIT			REPAIR AND RETROFIT		
BMP ID	OR GEN		OWNER NAME:		
FILE NUMBER: WC046		WC046			WJCC SCHOOLS
PIN:	IN: 1310100020			SITE ADDRESS:	3651 ROCHAMBEAU DRIVE
				LEGAL	STONEHOUSE ELEMENTARY;GEORGE M
				DESCRIPTION:	HANKINS ELEMENTARY SCHOOL #7
					SITE

MAINTENANCE					
AGREEMENT IN		BOOK/PAGE OR		OTHER	
FILE:	N/A	DOCUMENT NO.:	N/A	DESCRIPTION:	N/A

BOX NO.:	2	COMMENTS:	TED ANICA AITTE A I
			TRANSMITTAL



TRANSMITTAL SHEET

ENGINEERING & RESOURCE PROTECTION \Rightarrow STORMWATER

Project: Stonehouse Elementary Stormwater Repair & Retrofit	
County Plan No.: SP-039-12	
Assigned BMP No: WC046	
BMP Type: <u>Dry Pond</u>	
Information Enclosed:	
X Computations	
X Other:	
Name: <u>Tina Creech</u>	
Date: 6/12/14	
Signature: <u>Oca Creed</u>	



James City County Engineering and Resource Protection Division Stormwater Management/BMP Record Drawing and Construction Certification Review Tracking Form

è Rebolit

Project Name: Stone house Elementary Stormwoter Repair
County Plan No. (List any amendments): SP-039-12
Stormwater Management Facility Type:
BMP Phase #: I I III VIII SIII
Information Package Submittal Date: 420114
Completeness Check: Record Drawing Date/By: Cardinal Surveying 2/27/K
Construction Certification Date/By: 155 41214
RD/CC Standard Forms (Ensure that all forms for the BMP type are included)
Ipsp/Maint Agreement # / Date: N (H
BMP Maintenance Plan Location: Sheet #5 @ SP-039-12
Special Considerations:
Standard E&SC Notes on Approved Plan Requiring RD/CC or County comment in plan review
Location (sheet #):
Log into Division's "As-Built Tracking Log"
Obtain basic site information (GPIN, Owner, Address, etc.)
Log into Access Database (BMP ID #, Plan No., GPIN, Project Name, etc.)
Copy from Active Project File (correspondence, H&H, design computations, etc.).
Create As-Built File using Project File information (File label, folder, copy plan/details/design
/information, etc.).
Inspector Review of RD/CC (consult with Chief Engineer prior to completion of comments).
Record Drawing Review against Approved Plan prior to Field Inspection.
Final Site Inspection (FI) Performed Date: 42514
Accord Browning (ND) Nevier
Construction Certification (CC) Review Date: 4/2/14
No comments.
Comments. Letter Forwarded. Date:
□ Record Drawing (RD)
□ Construction Certification (CC)
□ Construction-Related (CR)
□ Site Issues (SI)
Other:
Resubmittal (# and date):
Re-inspection (if necessary):
Complete "Surety Request Form".
Final Inspection of active file copying any relevant information to "As-Built" file.
On County BMP Inventory (Phase I, II or III).
Copy Final Inspection Report into County BMP Inspection Program file.
Provide Digital Photographs of BMP and save into County BMP Inventory.
Request mylar/reproducible from As-Built plan preparer.
Complete "As-built Tracking Log".
 ✓ Last check of BMP Access Database (County BMP Inventory). □ Add BMP to JCC Hydrology & Hydraulic database (optional).
 □ Add BMP to JCC Hydrology & Hydraulic database (optional). □ Add BMP to Municipal BMP list (if a County-owned facility)
Add BMP to PRIDE BMP ratings database.
Final Sign-Off
Inspector: Dia Viet Date: 6/12/14
Chief Engineer: Date: 06/14
*** See separate checklist, if needed.



Stormwater Management/BMP Facilities Record Drawing and Construction Certification Forms

(Note: In accordance with the requirements of the Chesapeake Bay Preservation Ordinance, Chapter 23, Section 23-10(4), BMP's shall be designed and constructed in accordance with the manual entitled James City County Guidelines for Design and Construction of Stormwater Management BMP's. Erosion and sediment control policy and approved plans generally require that at the completion of the project and prior to release of surety, an "as-built" plan prepared by a registered Professional Engineer or Certified Land Surveyor must be provided for the drainage system for the project, including any Best Management Practice (BMP) facilities. In addition, for BMP facilities involving the construction of an impounding structure or dam embankment, certification is required by a Professional Engineer who has inspected the structure during its construction. Currently there are over 20 water quality type BMP's accepted by the County.)

Section 1 - Site Information:

Project Name: Stonehouse Elementary School Stormwater Facility Repair/Retrofit
Structure/BMP Name: WC046
Project Location: Stonehouse Elementary School
BMP Location: 3651 Rochambeau Drive (west side of school)
County Plan No.: <u>SP-0039-2012</u>
Project Type: Residential Commercial Industrial Public Other Other Residential Business Tax Map/Parcel No.: 1310100020 BMP ID Code (if known): WC046 Zoning District: Public Lands Land Use: Elementary School Site Area (sf or acres): 26.22 acres
Brief Description of Stormwater Management/BMP Facility: The BMP is an existing dry detention facility that failed. This project involved rebuilding the dam and creating a constructed wetlands in the bottom of the basin with a micropool and berms to created extended flow paths for the stormwater in the basin.
Nearest Visible Landmark to SWM/BMP Facility: West side of the Stonehouse Elementary School
Nearest Vertical Ground Control (if known):
☐ JCC Geodetic Ground Control ☐ USGS ☐ Temporary ☐ Arbitrary ☐ Other
Station Number or Name:
Datum or Reference Elevation:
Control Description:
Control Location from Subject Facility:

Section 2 - Stormwate	er Management/BMP Facility Construction Information:
Approx. Construction S Facility Monitored by Name of Site Work Co Name of Professional I Date of Completion for	ing Held for Construction of SWM/BMP Facility: Yes No Unknown Start Date for SWM/BMP Facility: October 2013 County Representative during Construction: Yes No Unknown Intractor Who Constructed Facility: JSG Corporation Firm Who Routinely Monitored Construction: ECS Mid-Atlantic, LLC TSWM/BMP Facility: November 9, 2013 (except for wetlands plantings) Ing/Construction Certification Submittal: April 2014 (following wetland plantings)
Stormwater Managem reviewed and approvention, acceptance	ng and Construction Certifications are required within thirty (30) days of the completion of the completion of the completion of the completion of the and/or BMP facility construction. Record Drawings and Construction Certifications must be the dead of the James City County Engineering and Resource Protection Division prior to final to and bond or surety release.)
Section 3 - Owner/De	signer/Contractor Information:
Owner/Developer: (Ne	ote: Site Owner or Applicant responsible for development of the project.)
	Name: James City County Stormwater Division (site owned by Wmbg-JCC School Board) Mailing Address: 5320 Palmer Lane, Suite 2A Williamsburg, VA 23188 Business Phone: 757-259-1442 Fax: 757-259-5833 Contact Person: Darryl Cook Title: Capital Projects Coordinator
Design Professional:	(Note: Professional Engineer or Certified Land Surveyor responsible for the design and preparation of plans and specifications for the Stormwater Management / BMP facility.)
	Firm Name: AES Consulting Engineers
	Mailing Address: 5248 OldeTowne Road, Suite 1
	Williamsburg, VA 23188
	Business Phone: <u>757-253-0040</u>
	Fax: <u>757-220-8994</u>
	Responsible Plan Preparer: Bob Cosby
	Title: Project Engineer Plan Name: Standbayes Florenters School Starmyyeter Facility Parair/Patrofit
	Plan Name: <u>Stonehouse Elementary School Stormwater Facility Repair/Retrofit</u> Firm's Project No. <u>W10119-E-04</u>
	Plan Date: 4/17/12 - final revision date 06/10/13
	Sheet No.'s Applicable to SWM/BMP Facility: 1 thru 5 ////
BMP Contractor: (Not	e: Site Work Contractor directly responsible for construction of the Stormwater Management/BMF facility.)
	Firm Name: JSG Corporation
	Mailing Address: PO Box 646
	Lightfoot, VA 23090
	Business Phone: 757-645-4870

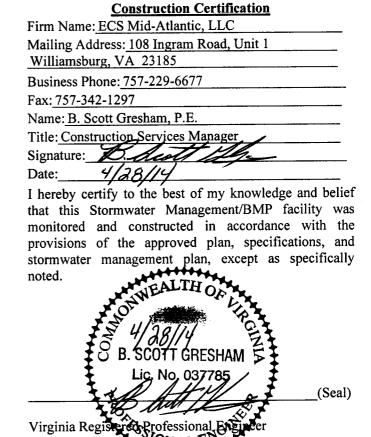
Fax: <u>757-645-4860</u>
Contact Person: Mike Mullins
Site Foreman/Supervisor: Mike Hubbard
Specialty Subcontractors and Purpose (for BMP Construction Only):
Shoreline Sensations - Wetlands plant installation (actually hired directly by James City County)

Section 4 - Professional Certifications:

Certifying Professionals: (Note: A Registered Professional Engineer or Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)

Record Drawing and Construction Certifications for Stormwater Management/BMP Facilities

Record Drawing Certification Firm Name: Cardinal Surveying and Design Mailing Address: 150 Strawberry Plains Road, Ste D Williamsburg, VA 23188 Business Phone: 757-345-2866 Fax: 757-345-2877 Name: GEORGE M. CUNHA Title: OWNER Signature: I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management/BMP facility. The facility appears to conform to the provisions of the approved design plan, specifications design, and stormwater management plan, except as specifically noted.



<u>Section 5 - Record Drawing and Construction Certification Requirements and Instructions:</u>

- Pre-Construction Meeting Provides an opportunity to review SWM/BMP facility construction, maintenance and operation plans and addresses any questions regarding construction and/or monitoring of the structure. The design engineer, certifying professionals (if different), Owner/Applicant, Contractor and County representative(s) are encouraged to attend the preconstruction meeting. Advanced notice to the Engineering and Resource Protection Division is requested. Usually, this requirement can be met simultaneously with Erosion and Sediment Control preconstruction meetings held for the project.
- A fully completed STORMWATER MANAGEMENT / BMP FACILITIES, RECORD DRAWING and CONSTRUCTION CERTIFICATION FORM and RECORD DRAWING CHECKLIST. All applicable sections shall be completed in their entirety and certification statements signed and sealed by the registered professional responsible for individual record drawing and/or construction certification.
- The Record Drawing shall be prepared by a Registered Professional Engineer or Certified Land Surveyor for the drainage system of the project including any Best Management Practices.
- **7** Construction Certification - Construction of Stormwater Management / BMP facilities which contain impoundments, embankments and related engineered appurtenances including subgrade preparation, compacted soils, structural fills, liners, geosynthetics, filters, seepage controls, cutoffs, toe drains, hydraulic flow control structures, etc. shall be visually observed and monitored by a Registered Professional Engineer or his/her authorized representative. The Engineer must certify that the structure, embankment and associated appurtenances were built in accordance with the approved design plan, specifications and stormwater management plan and standard accepted construction practice and shall submit a written certification and/or drawings to the Engineering and Resource Protection Division as required. Soil and compaction test reports, concrete test reports, inspection reports, logs and other required construction material or installation documentation may be required by the Engineering and Resource Protection Division to substantiate the certification, if specifically requested. The Engineer shall have the authority and responsibility to make minor changes to the approved plan, in coordination with the assigned County inspector, in order to compensate for unsafe or unusual conditions encountered during construction such as those related to bedrock, soils, groundwater, topography, etc. as long as changes do not adversely affect the integrity of the structure(s). Major changes to the approved design plan or structure must be reviewed and approved by the original design professional and the James City County Environmental Division.
- Record Drawing and Construction Certifications are required within **thirty (30) days** of the completion of Stormwater Management / BMP facility construction. Submittals must be reviewed and accepted by James City County Engineering and Resource Protection Division prior to final inspection, acceptance and bond/surety release.

Dual Purpose Facilities - Completion of construction also includes an interim stage for Stormwater Management / BMP facilities which serve dual purpose as temporary sediment basins during construction and as permanent stormwater management / BMP facilities following construction, once development and stabilization are substantially complete. For these dual purpose facilities, construction certification is required once the temporary sediment basin phase of construction is complete. Final record drawing and construction certification of additional permanent components is required once permanent facility construction is complete.

Interim Construction Certification is required for those dual purpose embankment-type facilities that are generally ten (10) feet or greater in dam height (*) and may not be converted, modified or begin function as a permanent SWM / BMP structure for a period generally ranging from six (6) to eighteen (18) months or more from issuance of a Land Disturbance permit for construction.

Interim or final record drawing and construction certifications are not required for temporary sediment basins which are designed and constructed in accordance with current minimum standards and specifications for temporary sediment basins per the Virginia Erosion and Sediment Control Handbook (VESCH); have a temporary service life of less than eighteen (18) months; and will be removed completely once associated disturbed areas are stabilized, <u>unless</u> a distinct hazard to the public's health, safety and welfare is determined by the Engineering and Resource Protection Division due to the size or presence of the structure or due to evidence of improper construction.

(*Note: Dam Height as referenced above is generally defined as the vertical distance from the natural bed of the stream or waterway at the downstream toe of the embankment to the top of the embankment structure in accordance with 4VAC50-20-30, Virginia Impoundment Structure Regulations and the Virginia Dam Safety Program.)

- Record Drawings shall provide, at a minimum, all information as shown within these requirements and the attached RECORD DRAWING CHECKLIST specific to the type of SWM/BMP facility being constructed. Other additional record data may be formally requested by the James City County Engineering and Resource Protection Division. (Note: Refer to the current edition of the James City County Guidelines for Design and Construction of Stormwater Management BMP's manual for a complete list of acceptable BMP's. Currently there are over 20 acceptable water quality type BMP's accepted by the County.)
- Record Drawings shall consist of blue/black line prints and a reproducible (mylar, sepia, diazo, etc.) set of the approved stormwater management plan including applicable plan views, profiles, sections, details, maintenance plans, etc. as related to the subject SWM / BMP facility. The set shall indicate "RECORD DRAWING" in large text in the lower right hand corner of each sheet with record elevations, dimensions and data drawn in a clearly annotated format and/or boxed beside design values. Approved design plan values, dimensions and data shall not be removed or erased. Drawing sheet revision blocks shall be modified as required to indicate record drawing status. Elevations to the nearest 0.1' are sufficiently accurate except where higher accuracy is needed to show positive drainage. Certification statements as shown in Section 4 of the Record Drawing and Construction Certification Form, or similar forms thereof, and professional signatures and seals, with dates matching that of the record drawing status in the revision or title block, are also required on all associated record drawing plans, prints or reproducibles.
- Submission Requirements Initial and subsequent submissions for review shall consist of a minimum of one (1) blue/black line set for record drawings and one copy of the construction certification documents with appropriate transmittal. Under certain circumstances, it is understood that the record drawing and construction certification submissions may be performed by different professional firms. Therefore, record drawing submission may be in advance of construction certification or vice versa. Upon approval and prior to release of bond/surety, final submission shall include one (1) reproducible set of the record drawings, one (1) blue/black line set of the record drawings and one (1) copy of the construction certification. Also for current and/or future incorporation into the County BMP database and GIS system,

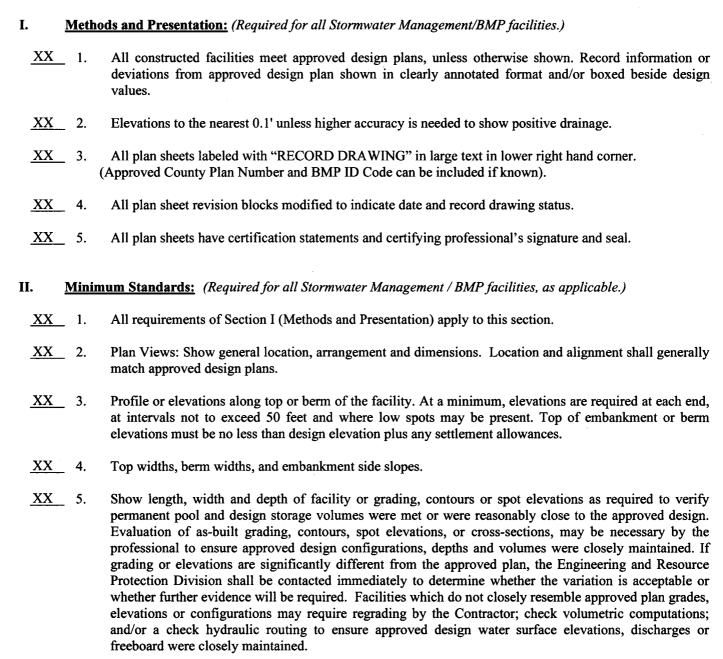
Stormwater Management/BMP Facilities Record Drawing and Construction Certification Forms

Page 6

it is requested that the record drawings also be submitted to the Engineering and Resource Protection Division on a diskette or CD-ROM in an acceptable electronic file format such as *.dxf, *.dwg, etc. or in a standard scanned and readable format. The electronic file requirement can be discussed and coordinated with Engineering and Resource Protection Division staff at the time of final submission.

STORMWATER MANAGEMENT/BMP FACILITIES RECORD DRAWING CHECKLIST

(Key for Checklist is as follows: XX Acceptable N/A Not Applicable Inc Incomplete)

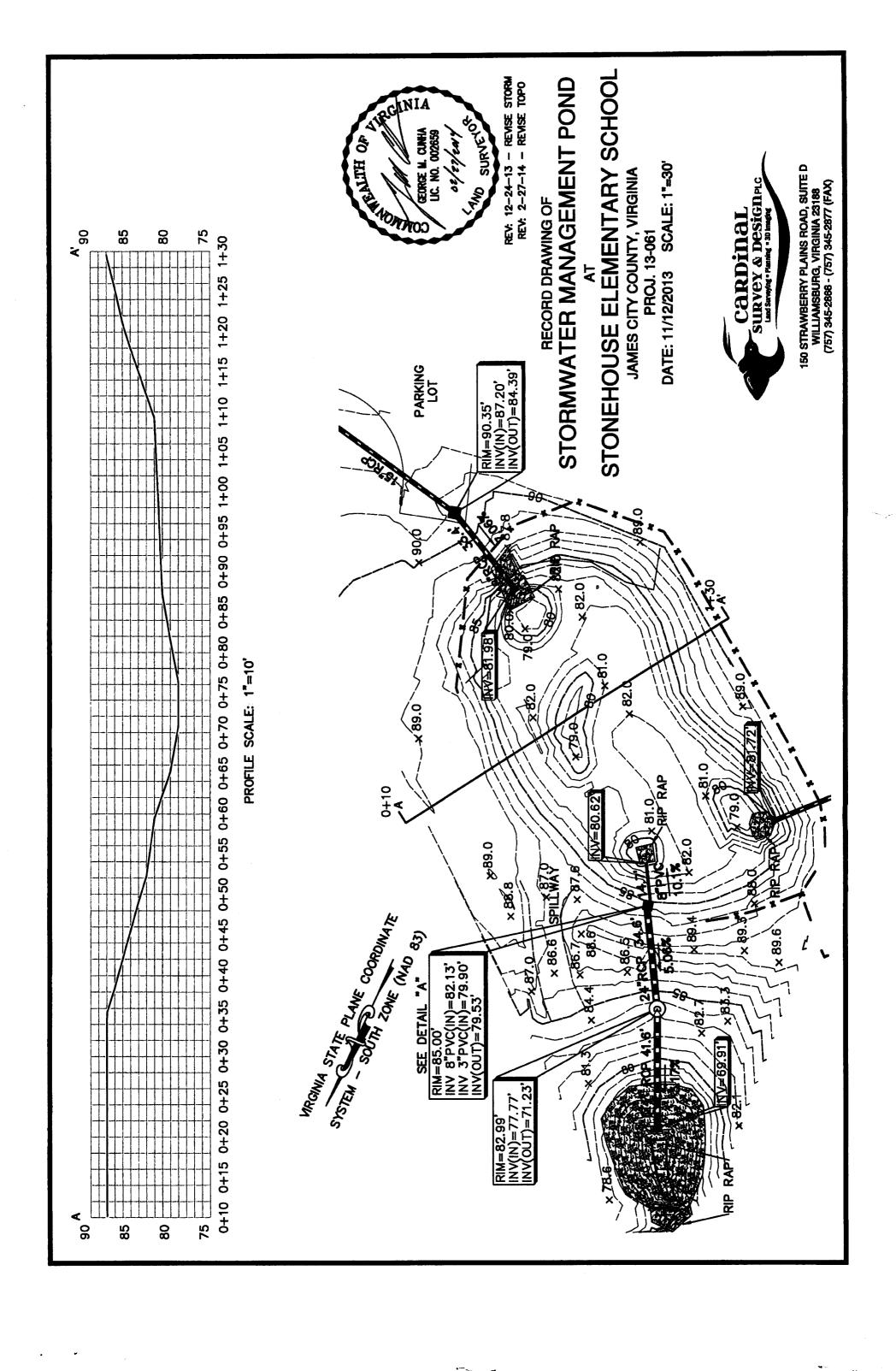


- 6. Cross-section of the embankment through the principal spillway or outlet barrel. Must extend at least 100 ft. downstream of the pipe outlet or to recorded site property line, whichever is closer. Proper correlation is required between principal spillway (control structure) crest, emergency spillway crest, orifice, and weirs and the top of the dam or facility. All elevations and dimensions must reasonably match the design plan or be sequentially relative to each other and the facility must reflect the required design storage volume(s) and/or design depth.
- XX 7. Profile or elevations along the entire centerline of the emergency spillway. Emergency spillway may be steeper, but no flatter or narrower than design.
- XX 8. Elevation of the principal spillway crest or outlet crest of the structure.
- <u>XX</u> 9. Primary control structure (riser) diameter or dimensions, height, type of material and base size. Indicate provisions for access that are present such as steps, ladders, etc.
- XX 10. Dimensions, locations and elevations of outlet orifices, weirs, slots and drains.
- XX 11. Type and size of anti-vortex and trash rack device. Height, diameter, dimensions, bar spacings (if applicable) and elevations relative to the principal spillway crest. Indicate if lockable hatch is present or not.
- XX 12. Type, location, size, and number of anti-seep collars or documentation of other methods utilized for seepage control. May need to obtain this information during construction.
- NA 13. Top of impervious core embankment, core trench limits and elevation of cut-off trench bottom. May need to obtain this information during construction.
- XX 14. Elevation of the principal spillway barrel (outlet pipe) inlet and outlet invert.
- XX 15. Outlet barrel diameter, length, slope, type, and thickness class of material and type of flared end sections, headwall or endwall.
- XX 16. Outfall protection dimension, type and depth of rock and if underlain filter fabric is present.
- XX 17. BMP interior and periphery landscaping zones conform with arrangements and requirements of the approved design plan.
- NA 18. Maintenance plan taken from approved design plan transposed onto record drawing set.
- XX 19. Fencing location and type, if applicable to facility.
- XX 20. BMP vicinity properly cleaned of stockpiles and construction debris.
- NA 21. No visual signs of erosion or channel degradation immediately downstream of facility.
- NA 22. Any other information formally requested by the Environmental Division specific to the constructed SWM/BMP facility.

STORMWATER MANAGEMENT/BMP FACILITIES RECORD DRAWING CHECKLIST

(Key for Checklist is as follows: XX Acceptable N/A Not Applicable Inc Incomplete)

- IV. Group B Wetlands (Includes B-1 Shallow Marsh; B-2 Ext Det Shallow Wetlands; B-3 Pond Wetland System and B-4 Pocket Wetland)
 - XX B1. Same requirements as Group A Wet Ponds.
 - XX B2. Minimum 2:1 length to width flow path provided across the facility.
 - XX B3. Micropool provided at or around outlet from BMP (generally 3 to 6 ft. deep).
 - XX B4. Wetland type landscaping provided in accordance with approved plan. Includes correct pondscaping zones, plant species, planting arrangements, wetland beds, etc. Wetland plants include 5 to 7 emergent wetland species. Individual plants at 18 inches on center in clumps.
 - NA B5. Adequate wetland buffer provided (Typically 25 ft. outward from maximum design water surface elevation and 15 ft. setback to structures).
 - XX B6. No more than one-half (½) of the wetland surface area is planted.
 - XX B7. Topsoil or wetland mulch provided to support vigorous growth of wetland plants.
 - <u>XX</u> B8. Planting zones staked or flagged in field and locations subsequently established by appropriate field surveying methods for record drawing presentation.



NOTES

1. EXISTING CONDITIONS SHOWN ON THIS PLAT ARE THE RESULT OF AN ON-THE-GROUND SURVEY PERFORMED BY THIS FIRM ON NOVEMBER 12, 2013. 1' CONTOUR INTERVAL.

2. THE LOCATIONS OF UNDERGROUND UTILITIES SHOWN ON THIS PLAT ARE BASED UPON FIELD OBSERVATIONS. THEY ARE NOT WARRANTED TO BE EXACTLY LOCATED, NOR IS IT WARRANTED THAT ALL UNDERGROUND UTILITIES OR OTHER STRUCTURES ARE SHOWN ON THIS PLAT.

VRGINIA STATE PLANE COORDINATE SYSTEM SOUTH ZONE - NAD (83) 3. HORIZONTAL DATUM:

NGVD-29 VERTICAL DATUM:

LEGEND

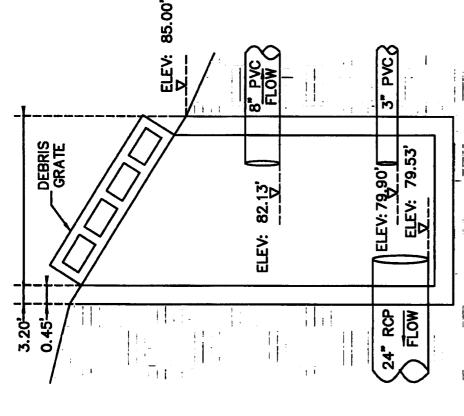
STORM SYSTEM PIPE

YARD DRAIN INLET STORM MANHOLE

× 12.3 EXISTING ELEVATION

---1' INTERVAL CONTOUR

-80-5' INTERVAL CONTOUR



SCALE: 1"=4000'

VICINITY MAP

ROCHMEAL

NOT TO SCALE DETAIL "A"

STORMWATER MANAGEMENT POND RECORD DRAWING OF

STONEHOUSE ELEMENTARY SCHOOL JAMES CITY COUNTY, VIRGINIA

PROJ. 13-061

SCALE: 1"=30

DATE: 11/12/2013

SURVEY & DESIGNPLC Land Surveying - 30 inaging carpinal

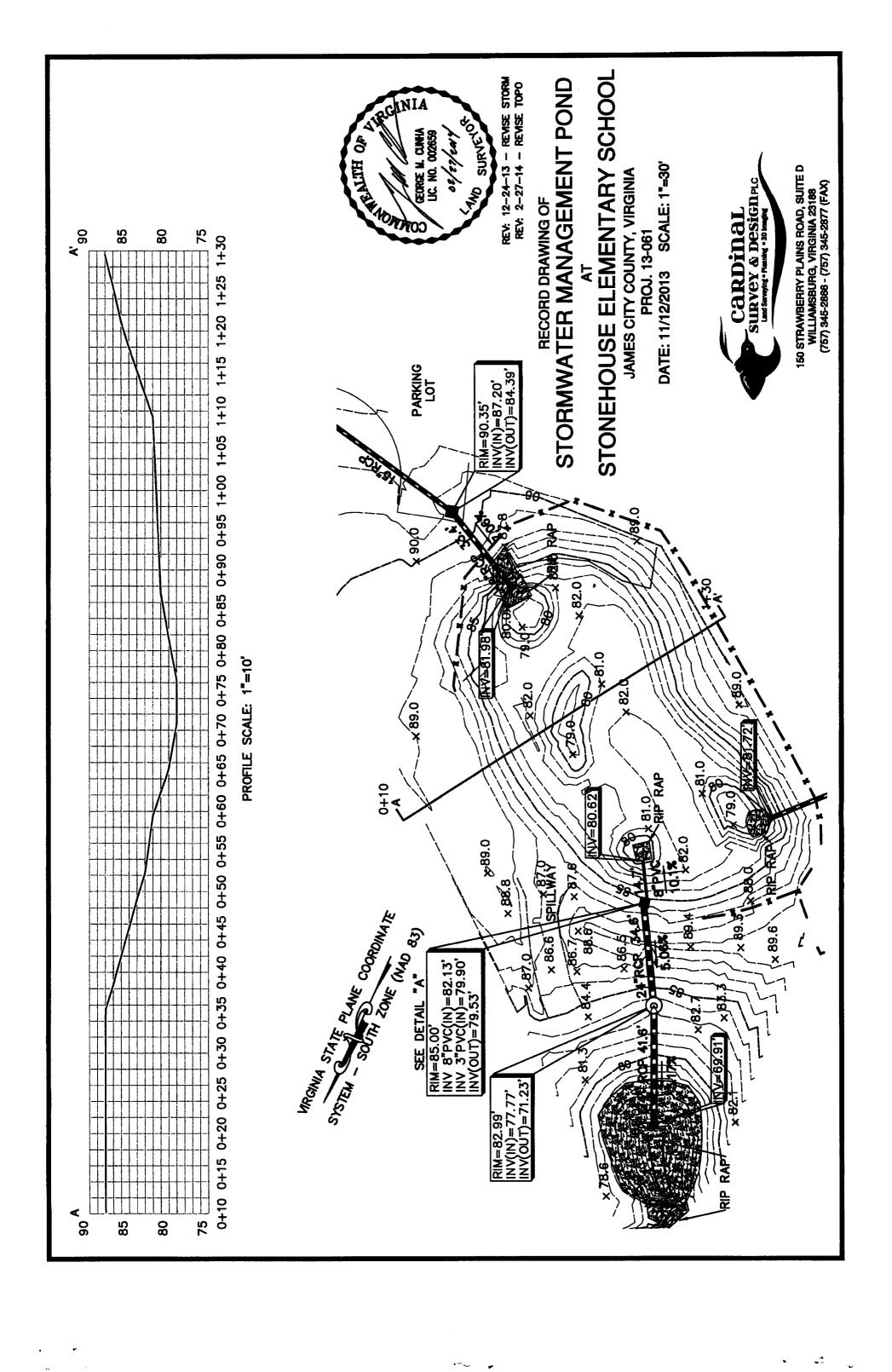
150 STRAWBERRY PLAINS ROAD, SUITE D WILLIAMSBURG, VIRGINIA 23188 (757) 345-2866 - (757) 345-2877 (FAX)

THIS PHYSICAL SURVEY HAS BEEN REVIEWED, AND IN MY PROFESSIONAL OPINION, BASED UPON MY KNOWLEDGE, INFORMATION, AND BELIEF, THE DESIGN ELEMENTS MEASURED BY THE PHYSICAL SURVEY COMPLY WITH THE APPROVED PLANS (EXCEPT AS SHOWN). THIS REVIEW DOES NOT IMPLY IN ANY WAY THAT;

INSPECTIONS WERE MADE DURING THE CONSTRUCTION, TO THE QUALITY OF THE WORK, OR TO ANY ELEMENT OR STRUCTURE NOT VISIBLE OR DEPICTED ON THE PHYSICAL SURVEY.

SO HITH THOMPOO CEORGE M. CUNHA LIC. NO. 002659 4102/22/30

REV: 12-24-13 - REVISE STORM REV: 2-27-14 - REVISE TOPO AND SURVEYOR



NOTES

1. EXISTING CONDITIONS SHOWN ON THIS PLAT ARE THE RESULT OF AN ON-THE-GROUND SURVEY PERFORMED BY THIS FIRM ON NOVEMBER 12, 2013. 1' CONTOUR INTERVAL.

DEBRIS GRATE

3.20 0.45

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VRGINIA STATE PLANE COORDINATE SYSTEM SOUTH ZONE — NAD (83) 3. HORIZONTAL DATUM:

NGVD-29 VERTICAL DATUM:

LEGEND

STORM SYSTEM PIPE

STORM MANHOLE 0

× 12.3 EXISTING ELEVATION YARD DRAIN INLET

-80-5' INTERVAL CONTOUR ---1' INTERVAL CONTOUR



VICINITY MAP SCALE: 1"=4000'

ROCHAMBEAL

ELEV: 85.00° Z_--

FLOW (

ELEV: 82.13°

NOT TO SCALE DETAIL "A"

RECORD DRAWING OF

STONEHOUSE ELEMENTARY SCHOOL STORMWATER MANAGEMENT POND

JAMES CITY COUNTY, VIRGINIA

SCALE: 1"=30" PROJ. 13-061 DATE: 11/12/2013



150 STRAWBERRY PLAINS ROAD, SUITE D WILLIAMSBURG, VIRGINIA 23188 (757) 345-2866 - (757) 345-2877 (FAX)

THIS PHYSICAL SURVEY HAS BEEN REVIEWED, AND IN MY PROFESSIONAL OPINION, BASED UPON MY KNOWLEDGE, INFORMATION, AND BELIEF, THE DESIGN ELEMENTS MEASURED BY THE PHYSICAL SURVEY COMPLY WITH THE APPROVED PLANS (EXCEPT AS SHOWN). THIS REVIEW DOES NOT IMPLY IN ANY WAY THAT;

SOUTH OF THE PLITH OF

SEORGE IN CUNHA LIC. NO. 002659

4102/12/20

INSPECTIONS WERE MADE DURING THE CONSTRUCTION, TO THE QUALITY OF THE WORK, OR TO ANY ELEMENT OR STRUCTURE NOT VISIBLE OR DEPICTED ON THE PHYSICAL SURVEY.

> REV: 12-24-13 - REVISE STORM REV: 2-27-14 - REVISE TOPO TWO SURVEYOR



Notes:

James City County Environmental Division Stormwater Management / BMP Inspection Report Detention and Retention Pond Facilities

County BMP ID Code (if I	known): 🚺	046		For \$1034.12 AP No.: 1 of 1 Date: 4	. 1				
Name of Facility:	rohou	ir Elem SO	REDOUTE BY	MP No.: of Date:	4/27/14				
Location: 3651 Rochambau De. Retrofit									
Name of Owner: WUCC									
Name of Inspector: TCreech - M. Lew. S									
Type of Facility: Dn	1 Pon	<u>d</u>	<u>.</u> .						
Weather Conditions:	unny	Type: D f	inal Inspection	County BMP Inspection Program	Owner Inspection				
If an inspection item is no	ot applicable	, mark NA, otherwise m	ark the appropriate	column.					
O.K The item checked is in adequate condition and the maintenance program is currently satisfactory. No action required. Routine - The item checked requires attention, but does not present an immediate threat to the function/integrity of the BMP. Urgent - The item checked requires immediate attention to keep the BMP operational and to prevent damage to the facility. Provide an explanation and details in the comment column, if routine or urgent are marked.									
Facility Item	о.к.	Routine	Urgent	Comm	ents				
Embankments and Side	e Slopes:								
Grass Height									
Vegetation Condition									
Tree Growth									
Erosion									
Trash & Debris									
Seepage									
Fencing or Benches									
Interior Landscaping/F	Planted Areas	s: None Deconstr	ucted Wetland/Shallo	ow Marsh	Vegetation				
Vegetated Conditions									
Trash & Debris									
Floating Material									
Erosion									
Sediment									
Dead Plant		/		- :					
Aesthetics									
Aesthetics									

Facility Item	О.К.	Routine	Urgent	Comments		
Water Pools: Permanent Pool (Retention Basin) Shallow Marsh (Detention Basin) None, Dry (Detention Basin)						
Shoreline Erosion						
Algae						
Trash & Debris						
Sediment						
Aesthetics	,					
Other						
Inflows (Describe Type	s/Locations):	1811 RC1				
Condition of Structure						
Erosion			-			
Trash and Debris						
Sediment		/				
Outlet Protection						
Other						
Principal Flow Control	Structure - 1	Riser, Intake, etc. (Descr	ibe Type):	"80P/48" Riser		
Condition of Structure						
Corrosion						
Trash and Debris						
Sediment						
Vegetation		,				
Other						
Principal Outlet Struct	ure - Barrel,	Conduit, etc. :	LY" ROP	-81PVC		
Condition of Structure						
Settlement						
Trash & Debris						
Erosion/Sediment						
Outlet Protection	V					
Other						
Emergency Spillway (Overflow):						
Vegetation						
Lining						
Erosion						
Trash & Debris						
Other						
Notes:						

		en e	-					
Facility Item	O.K.	Routine	Urgent	Comments				
Nuisance Type Conditions:								
Mosquito Breeding								
Animal Burrows	<u></u>							
Graffiti								
Other								
Surrounding Perimeter	Conditions:							
Land Uses	<i>'</i>			JCCSohool				
Vegetation	1							
Trash & Debris								
Aesthetics								
Access /Maintenance Roads or Paths	·							
Other Fence				Locked				
Remarks:		-						
Overall Environmental Division Internal Rating:								
Colon Day a Colon Division and the Adding.								
Signature: Date: 42114								
Title:								

SWMProg\BMP\CoInspProg\InspForms\DetRet.wpd

Tina Creech

From: Darryl Cook

Sent: Monday, October 07, 2013 4:34 PM

To: Mike Mullins (michael.mullins@jsgcorp.com); mike.hubbard@jsgcorp.com

Cc: David Greshamer; Tina Creech

Subject: Stonehouse Elementary School BMP Repair

Regarding two of the items discussed this morning, I wanted to document the decisions. Concerning the stilling basin location, I agreed to a relocation of it 15 feet upstream (closer to the embankment). All the dimensions of the stilling basin will remain the same. At the end of the project, the existing riprap check dam will be flattened out and used to protect the channel below the stilling basin to as close to the property line as the amount of stone will allow. The reason for the change is to reduce land disturbance as the further down the ravine, the steeper and narrower it becomes.

Concerning increasing the drop in the new manhole structure (SS#1-2) to reduce the slope of the outlet pipe, that is also acceptable as long as a minimum pipe slope of 4% is maintained on the outlet pipe. The slope of the existing barrel pipe, which was 3.6%, was used in the design of the pond. So as long as the slope is greater than 3.6% (I suggested 4% to make it a simpler calculation but it probably doesn't matter these days), then the change in slope and the drop in the structure is acceptable. One additional consideration is that the new barrel pipe needs to be laid at a slope of at least 3.6% to meet the original design calculations.

I still need to look into the trash rack issue. Let me know if you need anything else.

Darryl E. Cook
Capital Projects Coordinator



General Services Department 5320 Palmer Lane, Suite 2A Williamsburg, VA 23188 P: 757-259-1442 F: 757-259-5833 jamescitycountyva.gov

Tina Creech

From:

Darryl Cook

Sent:

Wednesday, September 25, 2013 1:07 PM

To:

Cc:

'mike.hubbard@jsgcorp.com'; Mike Mullins (michael.mullins@jsgcorp.com); 'SGresham'

(SGresham@ecslimited.com); Tina Creech; David Greshamer

Bob Cosby

Subject:

Stonehouse ES BMP - Pipe Bedding

I spoke to Bob Cosby with AES and it was their intention that bedding <u>not</u> be provided below the concrete pipe. If there are problems with the soil for the pipe to be installed in the area below the dam, then up to 4 inches of #57 stone can be provided but no stone should be placed under the pipe within the dam section.

1

Darryl E. Cook Capital Projects Coordinator



General Services Department 5320 Palmer Lane, Suite 2A Williamsburg, VA 23188 P: 757-259-1442 F: 757-259-5833



REPORT OF

SUBSURFACE EXPLORATION AND GEOTECHNICAL ENGINEERING ANALYSIS

STONEHOUSE ELEMENTARY SCHOOL BMP SPILLWAY REPAIR JAMES CITY COUNTY, VIRGINIA

ECS MID-ATLANTIC, LLC PROJECT NO. 07:10665

For

Mr. Barry Moses, P.E.
James City County Stormwater Division
287 McLaws Circle Suite 1
Williamsburg, VA 23185-5649

June 29, 2010

SP-39-12

O ADORESSES CINDITION OF EMBANKMENT E SPILLWAY + PROP. REPAIR WORK

o loes not address
pond storage area
ability to hold
water in wetlands.



June 29, 2010

Mr. Barry Moses, P.E. James City County Stormwater Division 287 McLaws Circle Suite 1 Williamsburg, VA 23185-5649

ECS Project No. 07:10665

Reference:

Report of Subsurface Exploration and Geotechnical Engineering Analysis

Stonehouse Elementary School BMP Spillway Repair

James City County, Virginia

Dear Mr. Moses:

ECS Mid-Atlantic, LLC (ECS) is pleased to submit this report of our subsurface exploration and geotechnical engineering analysis for the above referenced project. The purpose of this investigation was to ascertain the nature of the erosion affecting the spillway pipe and embankment, develop recommendations for repairs, and provide earthwork specifications for the project.

ECS accomplished these purposes by drilling soil test borings and analyzing the soil samples from the borings to evaluate pertinent engineering properties. On this basis we developed our geotechnical engineering recommendations. No other warranties are expressed or implied.

The conclusions and recommendations contained in this report are based upon a total of two (2) soil test borings drilled to depths of 20 feet below the existing grades, a site reconnaissance performed by an ECS engineer, and laboratory test results of boring samples. The borings were located in the field by ECS personnel in the immediate vicinity of the spillway pipe. The recommendations contained herein were developed from the data obtained in the soil borings which indicate subsurface conditions at these specific locations at the time of the exploration. Subsurface conditions may vary between the borings. If during the course of construction variations appear evident, the Geotechnical Engineer should be informed so that the conditions can be addressed. Geotechnical design recommendations were developed based on the project characteristics described herein. Should actual project characteristics differ from those discussed herein, this company should be informed such that a review of these characteristics can be performed.

Stonehouse Elementary School BMP Spillway Repair ECS Project No. 07:10665 Page 3

Project Characteristics

The project site consists of a wet detention pond comprising part of the stormwater management system for Stonehouse Elementary School. The pond was created by excavation of the impoundment and construction of an approximately 10 to 15-foot high dam embankment. The principal spillway consists of a pre-cast, grated inlet with a concrete pipe extending to a flared outlet. There has been considerable ground subsidence on the upstream face of the embankment just above the inlet and erosion of the downstream face of the dam embankment around the outlet pipe. A sink hole has developed above the pipe on the crest of the dam. It is not known if the pipe is leaking, allowing embankment soils to erode into the pipe, or if piping is causing erosion around the pipe. However, the erosion appears progressive.

Investigative Procedures

An ECS engineer performed a reconnaissance of the site prior to mobilization of the drill crew. Two (2) soil test borings were performed on this site on June 1, 2010. The borings were performed from the dam crest on either side of the spillway pipe. The borings were extended to a depth of 20 feet. The borings were performed with an ATV drill rig which utilized continuous-flight, solid-stem augers to advance the boreholes. Drilling services were provided by SDS, LLC of Toano, Virginia. Boring locations are indicated on the Boring Location Diagram included as Enclosure I of this report.

Representative samples were obtained by means of the split-barrel sampling procedure in accordance with ASTM Specification D-1586. In this procedure, a 2 inch O.D., split barrel sampler is driven into the soil a distance of 24 inches by a 140-pound hammer falling 30 inches. The number of blows required to drive the sampler through a 12-inch interval is termed the Standard Penetration Test (SPT) value and is indicated for each sample on the boring logs. This value can be used as a qualitative indication of the inplace relative density of cohesionless soils. In a less reliable way, it also indicates the consistency of cohesive soils. This indication is qualitative, since many factors can significantly affect the Standard Penetration resistance value and thus prevent a direct correlation between drill crews, drill rigs, drilling procedures, and hammer-rod-sampler assemblies. Samples were taken continuously to a depth of 10 feet and at 5-foot intervals thereafter. After recovery, representative portions of each sample were removed from the sampler and sealed in glass jars.

An experienced Geotechnical Engineer visually classified each soil sample from the borings on the basis of texture and plasticity in accordance with the Unified Soil Classification System (USCS) and ASTM D2488 (Description and Identification of Soils-Visual/Manual Procedures). The group symbols for each soil type are indicated in parentheses following the soil descriptions on the boring logs. The Geotechnical Engineer grouped the various soil types into the major zones noted on the boring logs of Enclosure II of this report. The stratification lines designating the interfaces between earth materials on the boring logs are approximate; in-situ, the transitions may be gradual.

A description of the Unified Classification System and Reference Notes for the boring logs are included in Enclosure III of this report.

Subsurface Conditions

The two soil borings were performed from the top of the dam embankment either side of the spillway pipe to ascertain the content and condition of the embankment fill in the vicinity of the spillway pipe and erosion features. Topsoil on the dam embankment was observed to be about 4 inches. In general, the dam

Stonehouse Elementary School BMP Spillway Repair ECS Project No. 07:10665 Page 4

embankment fill was observed to be about 8 feet deep and consisted primarily of Silty, fine SANDS (SM) of loose to medium dense relative density. Between 4 and 6 feet in B-1 and 2 and 4 feet in B-2, the Sands contained appreciable amounts of Clay. However, a Clay core was not encountered. Natural materials underlying the dam embankment consisted of deposits of Silty to Clayey to relatively clean, fine and fine to medium SANDS (SM, SM-SC, and SP) of medium dense relative density.

Observations for groundwater were made during sampling and upon completion of the drilling operations at each boring location. In auger drilling operations, water is not introduced into the boreholes, and the groundwater position can often be determined by observing water flowing into or out of the boreholes. Furthermore, visual observation of the soil samples recovered during the auger drilling exploration can often be used in evaluating the groundwater conditions. A groundwater table was not encountered by the 20-foot deep borings. Soils between 8 feet and 12 to 17 feet were very moist, while the soils below 12 to 17 feet were only moist, suggesting the spillway pipe is not submerged in a general seepage path through the embankment.

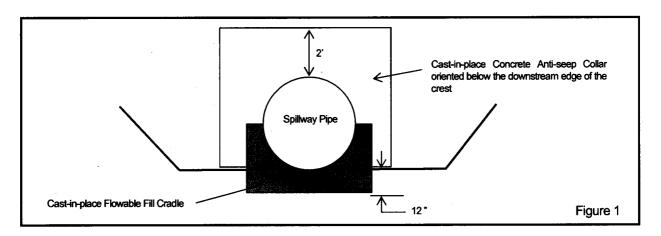
Conclusions

- 1. It does not appear that the spillway pipe is submerged below the level of the general seepage plane through the embankment. Given the granular nature of the foundation soils, seepage paths from the impoundment may actually be oriented more vertically downward from the pond bottom than horizontally through the embankment. In this regard, there would not be a strong tendency for piping along the sides of the spillway pipe, assuming well compacted soils were present around the pipe. Considering this, we expect it is most likely that water is moving from the impoundment to the outlet through relatively loose soils around the pipe, resulting in erosion around the pipe and collapse of overlying embankment fill materials.
- 2. It was not within the scope of this investigation to determine whether anti-seep devises, such as antiseep collars, are present. If present, they do not appear to be effective given the soil types which comprise the embankment.
- 3. It is possible that erosion around the pipe or consolidation of loose foundation soils below the pipe may have resulted in pipe deflection and loss of joint integrity. However, this was not explored within the scope of this investigation.
- 4. The borings do not indicate the presence of a Clay core, which would be employed in a zoned earth embankment. Nor do the embankment soils (Sands) appear to possess a sufficiently low permeability to be considered suitable for a homogeneous earth embankment. However, given the relatively small elevation difference between the impoundment's normal pool and the dam toe, this does not appear to be compromising the embankment's stability. The presence of relatively porous soils would make the spillway pipe subject to development of piping, particularly if soils around the pipe were not well compacted. Therefore, the repair plan should include replacement of soils around the pipe with Clayey soil material.

Embankment Repair Recommendations

1. To facilitate repair to the spillway, we recommend the pond be drained and the spillway pipe exposed in an excavation at least 3 feet wider than the pipe either side of the pipe at its invert elevation and with side slopes of 2H:1V or flatter.

- 2. Once exposed, the pipe should be inspected for settlement and loss of joint integrity. If excessive settlement has occurred, as defined by the County's Civil Engineering consultant, the affected pipe segments should be reset and joint seals repaired, as necessary.
- 3. In order to provide a competent base for the pipe and to help minimize piping along the pipe, we recommend that the pipe be supported by a Flowable Fill cradle extending from the upstream face of the dam embankment to the downstream outlet. The cradle should be at least 12 inches wider than the pipe either side of the pipe and 12 inches thick below the pipe. It should extend up to at least the pipe spring line or haunches (mid-point). The cradle should be cast in place against the pipe bottom surface, and the sides of the cradle should be cast against the sides of a trench excavated to facilitate its placement. The cradle need not be poured continuously. The pipe sections should be anchored as necessary to prevent floating.
- 4. In order to help protect against piping along the horizontal spillway pipe, we recommend that the horizontal spillway pipe be provided with one, cast-in-place concrete anti-seepage collar, as indicated in Figure 1 below. The collar should be at least 12 inches thick and extend beyond the top and side surfaces of the culvert at least 2 feet. The collar need not extend below the pipe cradle. The collar should be positioned below the downstream edge of the crest.



- 5. It is recommended that the dam repair section be constructed as a homogeneous earth embankment; that is, the repair cross section will not contain a distinct core and cover. Soil fill used in the repair section should satisfy the criteria for Embankment Fill discussed in the next section. We recommend the new embankment have side slopes no steeper than the existing embankment and a crest width of no less than the existing embankment.
- 6. In order to allow for seepage around the outlet, we recommend that the embankment surface within 3 feet beside and 1 foot above the outlet structure be covered with a non-woven filter fabric, a 6-inch layer of No. 3 Stone, and a 12-inch layer of Class II rip rap.

Construction Recommendations

- 1. Prior to initiation of earthwork operations, the pond should be drained so that water does not flow into the excavation.
- Subgrade preparation should include removal of any unsuitable material or excessively loose
 or porous soils from below the pipe cradle excavation bottom. The Geotechnical Engineer
 should be called on to observe all pipe support subgrades prior to backfilling to assure that
 competent foundation materials have been exposed.
- 3. It is essential that the side slopes of the repair section be laid back for safety as well as to allow compaction equipment to thoroughly compact Embankment Fill at the new fill-existing embankment interface. In this regard, the work area should be benched level and the side slopes graded to a maximum slope of 2H:1V, or flatter if necessary for safety.
- 4. Fill used to reconstruct the dam embankment around the spillway pipe (Embankment Fill) should consist of an inorganic soil material classified as SC, CL, or CH containing at least 40% fines (Silt and Clay). Maximum rock size should be limited to 6 inches. Any concentrations of rock material which impede compaction of the fill or which create void space in the fill should be removed. Silty Sands (SM and SP-SM) as well as clean Sands (SP) are not suitable for use in the dam embankment. In this regard, we recommend that material excavated from the existing dam not be reused in the repair section. Materials which are suitable as Embankment Fill will require importation from off-site sources or borrowing from suitable on-site sources, if available. No investigation of the suitability or location of potential on-site borrow materials has been performed as part of this study. The Geotechnical Engineer should be called on to evaluate materials proposed for use as Embankment Fill to assure they are suitable.
- 5. All Embankment Fill should be placed in maximum 8-inch loose lifts (4 inches for light compaction equipment) and moisture conditioned to within +/- 3% of the soil's optimum moisture content prior to compaction. Compaction should be accomplished using sheepsfoot and, if necessary, smooth drum rollers until a minimum density of 95% of the soil's Standard Proctor maximum dry density (ASTM D698) is achieved. Care should be exercised to achieve thorough compaction around structures using hand tampers. Thin fill lifts and hand tampers should be used against the sides of the pipe and around the anti-seep collar to assure that the

fill is adequately compacted. The side slopes of the repair section are to be sloped at 2H:1V or flatter. The purpose of this is to allow compaction equipment to roll from fill area to slope and compact within the transition zone between the two. A qualified Soils Technician under the direction of a Geotechnical Engineer should be called on to provide compaction testing during the fill placement to assure that the minimum compaction requirements are being met. At least 1 test per per lift should be performed.

Stonehouse Elementary School BMP Spillway Repair ECS Project No. 07:10665 Page 7

6. Dam maintenance is an essential requirement for assuring that dams perform as intended over time. The embankment should be periodically inspected for indications of seepage and erosion. Trees and brush should be removed from the embankment and should be kept from growing on the embankment, heavy grass growth should be maintained, and animal burrows should be filled. Pipes should be inspected for indications of leakage or for the presence of sediment, which might indicate leakage. If deterioration which might compromise the performance or safety of the dam is observed, a qualified Geotechnical Engineer should be called on to assist in the repair.

Closing

We appreciate the opportunity to be of service to you on this project. Should you have questions concerning this investigation, or if we can provide construction testing and inspection services, please contact our office.

Respectfully,

ECS Mid-Atlantic, LLC

Robert C. Moss, III, P.E.

Principal Engineer

ROBERT C. MOSS, III Lic. No. 019982

Michael J. Galli, P. E. VP, Branch Manager

Enclosures:

I. Boring Location Diagram

II. Soil Boring Logs

III. Unified Soil Classification System and Reference Notes for Boring Logs

IV. Summary of Laboratory Test Data

Copies:

(1) Client via email [BMoses@james-city.va.us]

Projects/2010/geotech/10665.doc

ENCLOSURES

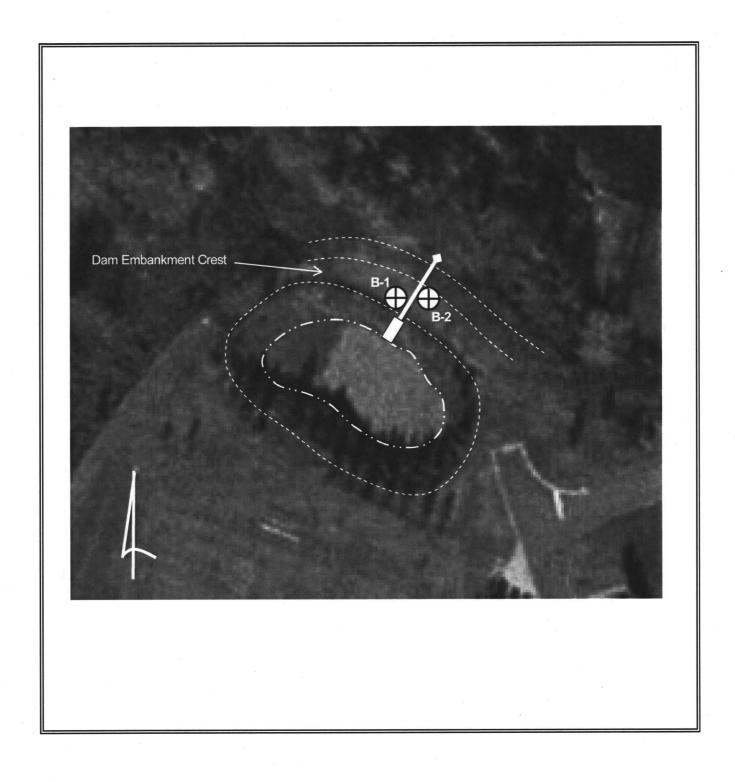
- I. Boring Location Diagram
- II. Soil Boring Logs
- III. Unified Soil Classification System and Reference Notes for Boring Logs
- IV. Summary of Laboratory Test Data

Enclosure I Boring Location Diagram

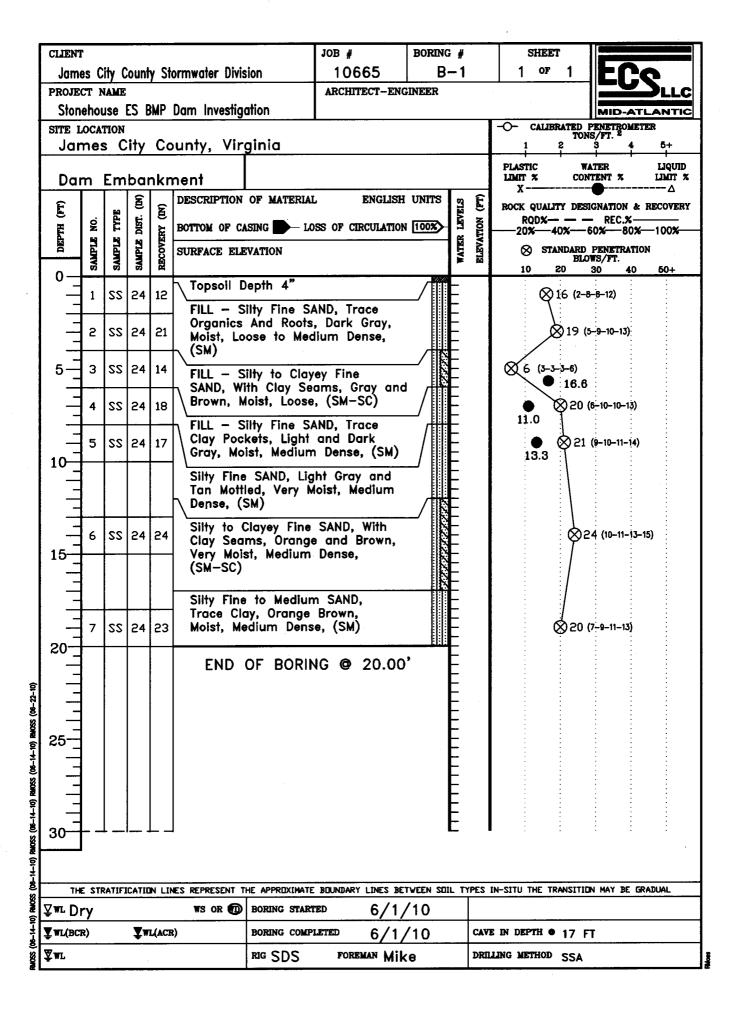
Enclosure I

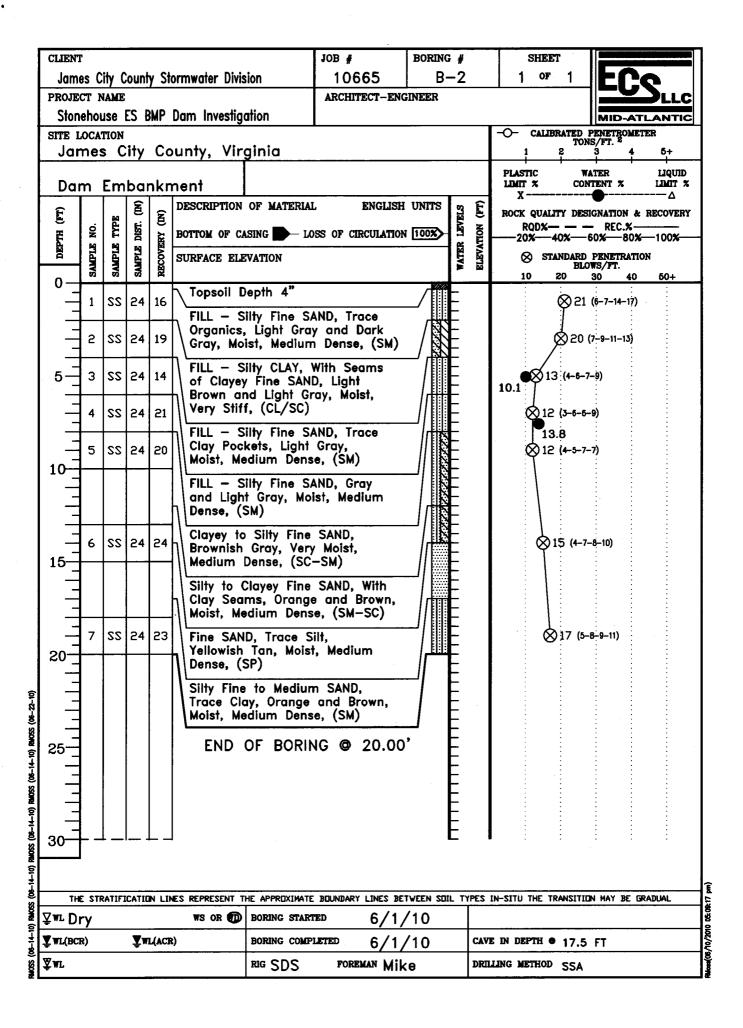
Boring Location Diagram

Stonehouse Elementary School BMP Spillway Repair James City County, Virginia ECS Mid-Atlantic, LLC Project No. 07:10665



Enclosure II
Soil Boring Logs





Enclosure III

Unified Soil Classification System and Reference Notes for Boring Logs

UNIFIED SOIL CLASSIFICATION SYSTEM (ASTM D-2487)

N	∕lajor Divis	ions	Grou Symb		Typical Names		Laboratory Classification Cr	riteria	
	. <u>s</u>	ravels or no is)	GW		Well-graded gravels, gravel- sand mixtures, little or no fines	soils	$C_u = D_{60}/D_{10}$ greater than 4 $C_c = (D_{30})^2/(D_{10}xD_{60})$ between 1	and 3	
	e fraction ve size)	Clean gravels (Little or no fines)	GP		Poorly graded gravels, gravel-sand mixtures, little or no fines	se-grained	Not meeting all gradation requi	rements for GW	
ained soils larger than No. 200 Sieve size)	Gravels (More than half of coarse fraction is larger than No. 4 sieve size)	Gravels with fines (Appreciable amount of fines)	GM ^e	d	Silty gravels, gravel-sand mixtures	Determine percentage of sand and gravel from grain-size curve. Depending on percentage of fines (fraction smaller than No. 200 sieve size), coarse-grained soils are classified as follows: Less than 5 percent GW, GP, SW, SP More than 12 percent GM, GC, SM, SC 5 to 12 percent Border 4 line cases requiring dual symbols ^b	Atterberg limits below "A" line or P.I. less than 4	Above "A" line with P.I. between 4 and 7 are borderline cases requiring use of dual symbols	
ined soils rger than No	(Mora Ia	Gravel (Apprecia	GC	<u> </u>	Clayey gravels, gravel-sand- clay mixtures	Determine percentage of sand and gravel from grain-size curve Depending on percentage of fines (fraction smaller than No. 200 are classified as follows: Less than 5 percent GW, GP, SW, SP More than 12 percent GM, GC, SM, SC 5 to 12 percent Border 4 line cases requiring dual symt	Atterberg limits below "A" line or P.I. less than 7 Atterberg limits below "A" line or P.I. less than 7 Cu = D ₆₀ /D ₁₀ greater than 6 Cc = (D ₃₀) ² /(D ₁₀ xD ₆₀) between 1 and 3 Not meeting all gradation requirements for SW Atterberg limits above "A" line or P.I. less than 4 Atterberg limits above "A" line Limits plotting or P.I. less than 4		
Coarse-grained soils laterial is larger than		sands or no	sw	/	Well-graded sands, gravelly sands, little or no fines	el from gra on smaller SP C C ses requir	$C_u = D_{60}/D_{10}$ greater than 6 $C_c = (D_{30})^2/(D_{10}xD_{60})$ between 1	and 3	
Coarse-gr More than half of material is I	e fraction eve size)	Clean sands (Little or no fines)	SP		Poorly graded sands, gravelly sands, little or no fines	f sand and gravel I fe of fines (fraction GW, GP, SW, SP GM, GC, SM, SC Border 4 line case	Not meeting all gradation requi	rements for SW	
(More than	Sands (More than half of coarse fraction is smaller than No. 4 sieve size)	ines nount o	SMª	d	Silty sands, sand-silt mixtures	tage of sanc centage of f ollows: nt GW, cent GM,	Atterberg limits above "A" line or P.I. less than 4	zone with P.I. between 4 and 7 are borderline cases requiring use of	
	fore than smaller t	Sands with fines (Appreciable amount o		u		Determine percentage o Depending on percentag are classified as follows: Less than 5 percent More than 12 percent 5 to 12 percent		dual symbols	
	(N	Sa (Appro	sc	;	Clayey sands, sand-clay mixtures	Determii Dependi are class Less tha More tha 5 to 12 p	Atterberg limits above "A" line with P.I. greater than 7		
	ays ss than		ML	_	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity		Plasticity Chart		
200 Sieve)	Silts and clays uid limit less th 50)	ilts and clays id limit less than 50)		CL CL CLays, sandy clays		50		"A" line	
an No.	Sil (Liqui		OL	-	Organic silts and organic silty clays of low plasticity			СН	
Fine-grained soils aterial is smaller th	rs er than		MH	1	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts	Plasticity Index	CL CL		
Fine-grained soils (More than half material is smaller than No.	Silts and clays (Liquid limit greater than 50)		CH	·	Inorganic clays of high plasticity, fat clays	10 Land	M	H and OH	
e than half	Si biupi⊥)		OH	1	Organic clays of medium to high plasticity, organic silts	o	CL-ML ML and OL	7 0 00 00 100	
(Mor	Highly Organic soils		Pt	1	Peat and other highly organic soils	0	10 20 30 40 50 60 Liquid Limit	70 80 90 100	

^a Division of GM and SM groups into subdivisions of d and u are for roads and airfields only. Subdivision is based on Atterberg limits; suffix d used when L.L. is 28 or less and the P.I. is 6 or less; the suffix u used when L.L. is greater than 28.

^b Borderline classifications, used for soils possessing characteristics of two groups, are designated by combinations of group symbols. For example:

GW-GC, well-graded gravel-sand mixture with clay binder. (From Winterkorn and Fang. 1975)

REFERENCE NOTES FOR BORING LOGS

I. Drilling Sampling Symbols:

SS	Split Spoon Sampler	ST	Shelby Tube Sampler
RC	Rock Core, NX, BX, AX	PM	Pressuremeter
DC	Dutch Cone Penetrometer	RD	Rock Bit Drilling
BS	Bulk Sample of Cuttings	PA	Power Auger (no sample)
HAS	Hollow Stem Auger	ws	Wash sample

II. Correlation of Penetration Resistances to Soil Properties:

Standard Penetration (blows/ft) refers to the blows per foot of a 140 lb. hammer falling 30 inches on a 2-inch OD split-spoon sampler, as specified in ASTM D-1586. The blow count is commonly referred to as the N value.

A. Non-Cohesive Soils (Silt, Sand Gravel and Combinations)

Dens	sity	Relative Properties				
Under 4 blows/ft	Very Loose	Adjective Form	12% to 49%			
4 to 10 blows/ft	Loose	With	5% to 12%			
11 to 30 blows/ft	Medium Dense					
31 to 50 blows/ft	Dense					
Over 51 blows/ft	Very Dense					

	Part	ticle Size Identification
Boulders		8 inches or larger
Cobbles		3 to 8 inches
Gravel	Coarse	1 to 3 inches
	Medium	½ to 1 inch
	Fine	1/4 to 1/2 inch
Sand	Coarse	2.00 mm to 1/4 inch (dia. of lead pencil)
	Medium	0.42 to 2.00 mm (dia. of broom straw)
	Fine	0.074 to 0.42 mm (dia. of human hair)
Silt and Clay		0.0 to 0.074 mm (particles cannot be seen)

B. Cohesive Soils (Clay, Silt, and Combinations)

Blows/ft	Consistency	Unconfined Comp. Strength Q _p (tsf)	Degree of Plasticity	Plasticity Index
Under 2	Very Soft	Under 0.25	None to slight	0 - 4
2 to 4	Soft	0.25-0.49	Slight	5 – 7
5 to 8	Medium Stiff	0.50-0.99	Medium	8 – 22
9 to 15	Stiff	1.00-1.99	High to Very High	Over 22
16 to 30	Very Stiff	2.00-3.00		
Over 30	Hard	Over 4.00		

III. Water Level Measurement Symbols:

WL	Water Level BCR	Before Casing Removal DCI	Dry Cave-In
WS	While Sampling ACR	After Casing Removal WCI	Wet Cave-In
WD	While Drilling	Existing Groundwater Level 7	Est. Seasonal High GWT

The water levels are those levels actually measured in the borehole at the times indicated by the symbol. The measurements are relatively reliable when augering, without adding fluids, in a granular soil. In clay and plastic silts, the accurate determination of water levels may require several days for the water level to stabilize. In such cases, additional methods of measurement are generally applied.

Enclosure IV Summary of Laboratory Test Data

Stonehouse Elementary School BMP Spillway Repair James City County, Virginia

ECS Mid-Atlantic, LLC Project No. 07:10665

Boring No.	Sample No.	Sample Depth (ft)	Natural Moisture Content (%)	Silt or Clay Content (%)	Unified Soil Classification
B-1	S-3	4-6	16.6	47.6	SM-SC
B-1	S-4	6-8	11.0	23.1	SM
B-1	S-5	8-10	13.3	29.9	SM
B-2	S-3	4-6	10.1	21.1	SM
B-2	S-4	6-8	13.8	27.1	SM

PLANNING DIVISION

DRAINAGE CALCULATIONS

JUN 17 2013

FOR

RECEIVED

STONEHOUSE ELEMENTARY

SITE: WC 046 BMP

James City County

SUBMITTED TO:

Environmental Division James City County

Prepared By:

AES Consulting Engineers 5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188

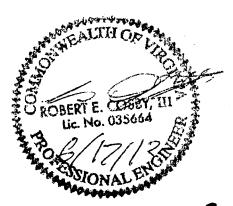
April 18, 2012 Revised June 17, 2013

AES Project No. W10119-E-04

W10119-E-04_Stormwater Management Report doc



RECEIVED



SP-39-12
FINALPS.

AIES

CONSULTING ENGINEERS

DRY POND TO WETLAND CONVERSION

TABLE OF CONTENTS

- -Stormwater Narrative
- -Manufactured Wetlands Pond Design
 - -SCS Calculations
 - Channel Protection Volume Calculations
 - -Hydrograph Report
 - -Anti-Seep Collar Design Calculations
 - -Outfall Storm System Calculations
 - -Outfall Storm System Outlet Protection Design
 - -Drainage Map
- -18" Existing Storm System Outlet Protection Design

STORM WATER NARRATIVE

F.2

B3 B4

PROJECT DESCRIPTION

This project involves the conversion of an existing dry pond into a constructed wetlands BMP at Stonehouse Elementary.

EXISTING SITE CONDITIONS

The existing site is a dry pond located in the northern corner of the Stonehouse Elementary School property.

ADJACENT PROPERTIES

The project is bordered on the northeast and northwest by wooded areas, on the southwest by grass field, and on the south by the school parking lot.

SOILS

The project area consists of 11C-Craven-Uchee complex and 19B Kempsville-Emporia Fine Sandy Loam with slopes ranging from 2 to 50 percent.

CRITICAL EROSION AREAS

There are areas of 25% slope impacts in this project. These amount to 0.166 acres or 25.9% of the total disturbed area.

STORMWATER MANAGEMENT & WATER QUALITY

Stormwater Management and water quality will be attained for this project through the use of the proposed Constructed Wetlands. The constructed wetlands consist of forebays at the locations of incoming pipes, deep pools that will remain wet, and the normal pool volume. Sizing of the facility is based on the Treatment Volume of 12,894 cubic feet. Of this volume, deep pool should provide 25% (3,224 cubic feet) and the normal pool should provide 50% (6,447 cubic feet). According to the Virginia DCR Stormwater Design Specification No. 13, deep pools consist of the deep wet pool, micropool, and forebay areas.

The proposed wetlands will provide 11,538 cubic feet of total treatment volume. The deep pools have a volume of 3,165 cubic feet. The normal pool includes the volume provided under elevation 83.22 which totals 5,120 cubic feet.

The channel protection volume required for the drainage area to the pond is 20,720 cubic feet. The channel protection volume provided is 24,609 cubic feet at the riser elevation of 85.26. An emergency spillway is provided at elevation 87.00 which will be utilized during 100-year storm events.

SCPV

Rip-rap outlet protection is provided at both the outfalls of the incoming pipes in the proposed wetlands. It is also provided at the outfall of the proposed storm system.

RESULTS & CONCLUSIONS

Due to the constraints of the existing pond design full compliance with the DCR technical specifications for a constructed wetlands can not be achieved. Specifically the 1 year Channel Protection Volume is provided, but at a depth greater than the 1 foot recommended. All other requirements regarding volume to be provided in the wet pool and extended detention volume are provided. Based on this analysis the new facility will have a higher pollutant removal efficiency as a constructed wetlands than the existing dry extended detention facility located on site. Therefore this facility as designed will improve the water quality benefits from the site, and maintain the water quantity controls consistent with the original facility.

GOOD BENEFIT

Stonehouse Elementary School Dam

CALCULATION FOR SCS HYDROGRAPH GENERATION AND CHANNEL PROTECTION

FOR Existing Pond

Project No. W10119-E-04 25-Feb-11

I. PRE-DEVELOPMENT CONDITIONS TO POINT OF CONCERN

A. Pre-Development Drainage Area to Point of Concern =

Pre-development Land Use, Soil Classification and Calculation of Composite Curve Number

7.39 Acres

Cuna

	Soil Type	Soil Hydrologic Group	Pre-Development Land Use	Area of Land Use (in Acres)	Number for Land Use (CN)	Adjusted (CN)
1)	Composite B/C Soils	С	Open Space (Good)	4.59	74	340
2)	Impervious Cover	N/A	Impervious Cover	2.8	98	274
3)					0	0
4)					0	0
5)					0	0
6)					0	0
7)	Impervious Cover		Impervious Cover		0	0
	Totals =			7.39		614
	Composite CN =					83

- C. Pre-Development Time of Concentration Calculations
 - 1) Overland Flow (maximum 300 feet)
 Surface description (table 5-7)
 Manning's roughness coefficient., n (table 5-7)
 Length of overland flow, L
 2-year 24-hour rainfall, P2
 Average slope of overland flow, s
 Travel time, Tt = (0.007*(n*L)^0.8)/(P2^0.5*s^0.4)
 - Shallow concentrated flow (maximum 300 feet) Surface description, paved or unpaved Length of shallow concentrated flow, L Average slope of shallow concentrated flow, s Average velocity, v Travet time, Tt = L/(3600°v)
 - 3) Channel or Pipe Flow Length of channel flow, L Average velocity of channel flow, v Travel time, Tt = L/(3600*v)

69

Total Time of Concentration =

Dense grasses 0.24 50 Feet 3.6 inches

50 Feet 3.6 inches 0.03 feet per foot 0.11 hours

unpaved
300 Feet
0.02 feet per foot
1.0 feet per second
0.08 hours

550 Feet 1.5 feet per second 0.10 hours

0.29 hours or 18 minutes

B-3 10pt. 1"perimperviocre

Forebay, bench, high/low, FB

07.39AC = 25,484 CF

B-4 6pt. 1"perimperviacre

For HWT/groundwater cases

DA = 13 28 AL.

IMPERV. 83

CN = 18 min.



Project:	Stonehouse Dam
Project No.:	W10119-04
Subject:	1 yr-24 hr Drawdown Calculation
	Kerplunk Method
Date:	3/9/2012 (Revised: 5/28/2013)
Calculated By:	GVC / REC

Channel Protection Volume:

Drainage Area

= 7.39 Acres

Runoff Curve No.

= 83 ×

1-Yr, 24-Hr Storm Volume

= 2.8 inches

Direct Runoff

(From TR55 Equations 2-3 & 2-4)

Q =

1.29 inches

Channel Protection Volume = DA x Q x 60%

(Virginia Stormwater Managment Handbook section 5-6.2 - Method 2)

ScpV

Vcp =

5.71 Ac-in

20,720 cubic feet

Determine Volume of Pond by Contour (starting at invert of low flow orifice):

Elevation	Incremental Depth	Area (sq. ft.)	Volume (cu. ft.)	Volume (cu. yd.)	Sum Volume (cu. ft.)	Sum Volume (cu. yd.)	Incremental Avg Head ¹ (feet)	Incremental Avg Flow ¹ (feet)	Incremental Drawdown Time¹ (hrs)
82.2	0.0	4,209	-	-	-	-			
83.0	0.8	7,787	4,678	173	4,678	173	0.39	0.12	10.68
84.0	1.0	8,684	8,236	305	12,914	478	1.28	0.25	9.01
85.0	1.0	9,617	9,151	339	22,064	817	2.21	0.34	6.36
86.0	1.0	10,595	10,106	374	32,170	1,191	0.00	0.00	0.00
87.0	1.0	11,973	11,284	418	43,454	1,609	0.00	0.00	0.00
88.0	1.0	14,395	13,184	488	56,638	2,098	0.00	0.00	0.00
	0.0		-	-	56,638	2,098	0.00	0.00	0.00
	0.0		-	-	56,638	2,098	0.00	0.00	0.00
	0.0		-	-	56,638	2,098	0.00	0.00	0.00
	0.0		-	-	56,638	2,098	0.00	0.00	0.00
		Total	56,638	2,098					26.05

¹ Incremental values computed from Channel Protection Volume Elevation

Elevation of Low Flow Orifice Invert Elevation of 1-yr, 24-hr Storage Volume Size of Orifice 82.22 feet 84.85 feet 3.00 inches

Total Average Drawdown Time

26.05 hrs

NOTE: MAINTAINING EXISTING LOW FLOW ORIFICE SIZE

72 1 host

Hydrograph Return Period Recap

Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

lyd.		Inflow				Hydrograph Description					
0.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-уг	50-уг	100-уг	pascuption
	SCS Runoff		10.95	15.93			33.23			50.07	Existing Drainage Area
2	Reservoir	1	0.634	1.425			15.81			41.50	Existing Pond Routed
4	Reservoir	1	0.382	1.451			16.47			42.29	Route 3 orifce
									ļ		
								:			
			:								
							<u>.</u>				
											•
								!			
							<u></u>		<u> </u>		

Proj. file: W10119-E-04_Existing Pond and Proposed Wetlands-REVISED-p5M26h22b/t,30gpW7, 2013

Hydrograph Summary Report
Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	10.95	2	724	34,533				Existing Drainage Area
2	Reservoir	0.634	2	838	34,496	1	84.67	24,054	Existing Pond Routed
4	Reservoir	0.382	2	962	34,489	1	84.96	26,771	Route 3 orifce
					i i				
	:								
						-			
						1			
		<u></u>							

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Monday, 00 17, 2013

= 10.95 cfs

= 724 min

= 83

= 0 ft

= 34,533 cuft

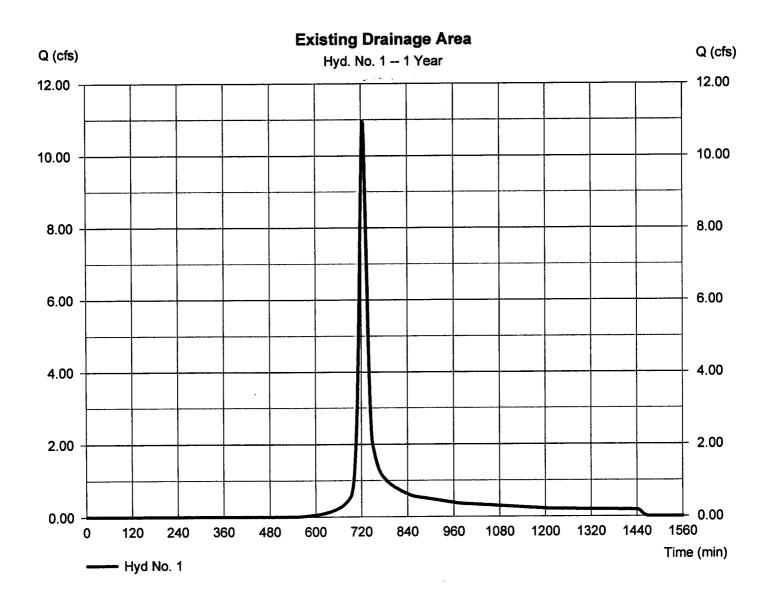
 $= 18.00 \, \text{min}$

Hyd. No. 1

Existing Drainage Area

Peak discharge = SCS Runoff Hydrograph type Storm frequency = 1 yrs Time to peak Hyd. volume Time interval = 2 min Curve number Drainage area = 7.390 acHydraulic length **Basin Slope** = 0.0 % Time of conc. (Tc) Tc method

Total precip. = 2.80 in Distribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

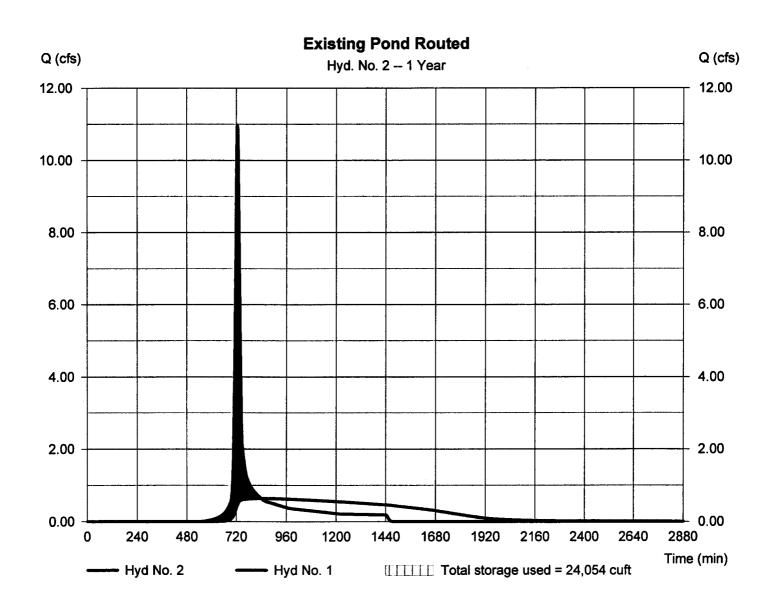
Monday, 00 17, 2013

Hyd. No. 2

Existing Pond Routed

Peak discharge = 0.634 cfsHydrograph type = Reservoir Time to peak Storm frequency = 838 min = 1 yrs Time interval = 2 min Hyd. volume = 34,496 cuftInflow hyd. No. = 1 - Existing Drainage Area Max. Elevation $= 84.67 \, \mathrm{ft}$ = Existing Pond Max. Storage = 24,054 cuftReservoir name

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.



Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Monday, 00 17, 2013

Pond No. 1 - Existing Pond

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 78.72 ft

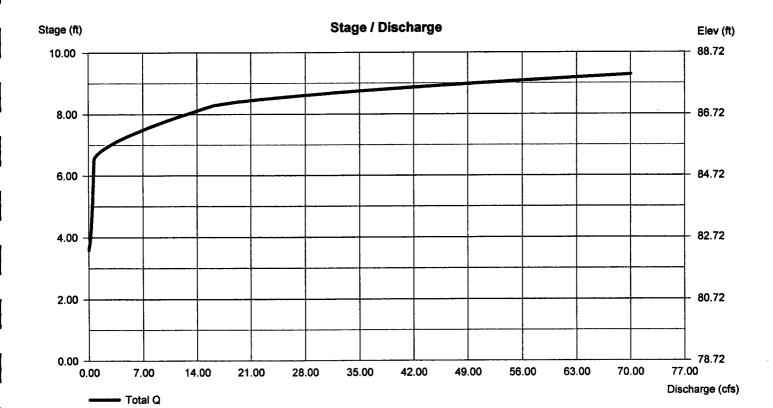
Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	78.72	304	0	0
1.00	79.72	719	497	497
2.00	80.72	1,235	965	1,462
3.00	81.72	1,851	1,532	2,995
3.28	82.00	4,209	826	3,821
4.28	83.00	7,787	5,906	9,727
5.28	84.00	8,684	8,231	17,958
6.28	85.00	9,617	9,146	27,103
7.28	86.00	10,595	10,101	37,204
8.28	87.00	11,973	11,276	48,480
9.28	88.00	14,395	13,164	61,644

Weir Structures Culvert / Orifice Structures [C] [D] [A] [B] [C] [PrfRsr] [A] [B] 0.00 = 2.0015.00 0.00 = 24.004.00 0.00 0.00 Crest Len (ft) Rise (in) 87.00 0.00 0.00 = 24.004.00 0.00 0.00 Crest El. (ft) = 85.26 Span (in) Weir Coeff. = 3.332.60 3.33 3.33 No. Barrels = 1 O O 1 **Broad** = Rect Invert El. (ft) = 79.06 82.22 0.00 0.00 Weir Type No No Length (ft) = 49.00 0.00 0.00 0.00 Multi-Stage = Yes No 0.00 0.00 n/a

= 3.63Slope (%) .013 .013 n/a **N-Value** = .013 = 0.000 (by Contour) Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = n/aYes No No TW Elev. (ft) = 0.00Multi-Stage

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

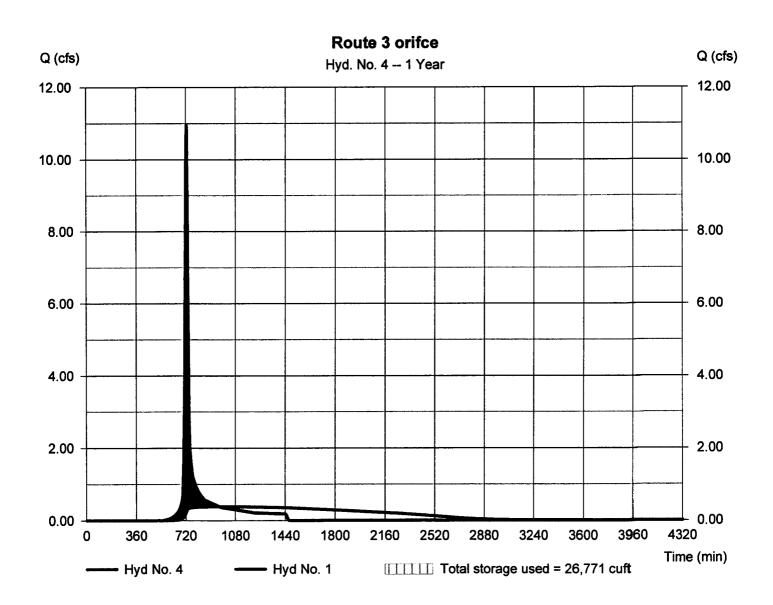
Monday, 00 17, 2013

Hyd. No. 4

Route 3 orifce

Peak discharge = 0.382 cfs= Reservoir Hydrograph type = 962 min Time to peak Storm frequency = 1 yrs Hyd. volume = 34,489 cuftTime interval = 2 min Max. Elevation $= 84.96 \, \mathrm{ft}$ Inflow hyd. No. = 1 - Existing Drainage Area Max. Storage 26,771 cuft Reservoir name = 3 orifice

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.



Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Monday, 00 17, 2013

Pond No. 2 - 3 orifice

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 78.72 ft

Stage / Storage Table

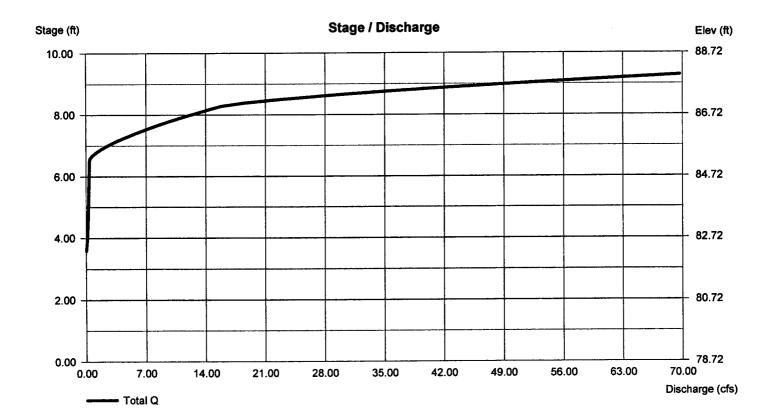
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	78.72	304	0	0
1.00	79.72	719	497	497
2.00	80.72	1,235	965	1,462
3.00	81.72	1,851	1,532	2,995
3.28	82.00	4,209	826	3,821
4.28	83.00	7.787	5,906	9,727
5.28	84.00	8,684	8,231	17,958
6.28	85.00	9,617	9,146	27,103
7.28	86.00	10.595	10,101	37,204
8.28	87.00	11,973	11,276	48,480
9.28	88.00	14,395	13,164	61,644

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	3.00	0.00	0.00	Crest Len (ft)	= 2.00	15.00	0.00	0.00
Span (in)	= 24.00	3.00	0.00	0.00	Crest El. (ft)	= 85.26	87.00	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	2.60	3.33	3.33
Invert El. (ft)	= 79.06	82.22	0.00	0.00	Weir Type	= Rect	Broad		
Length (ft)	= 49.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 3.63	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (b	y Contour)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydrograph Summary Report
Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	15.93	2	724	49,857				Existing Drainage Area
2	Reservoir	1.425	2	782	49,820	1	85.48	31,929	Existing Pond Routed
4	Reservoir	1.451	2	780	49,813	1	85.55	32,615	Route 3 orifce
									·
W1	W10119-E-04_Existing Pond and ProposedR WetlanderReEW2SE£a r05-28-20						3 Manuelay, 0	0 17, 2013	

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

= 24 hrs

Monday, 00 17, 2013

= 484

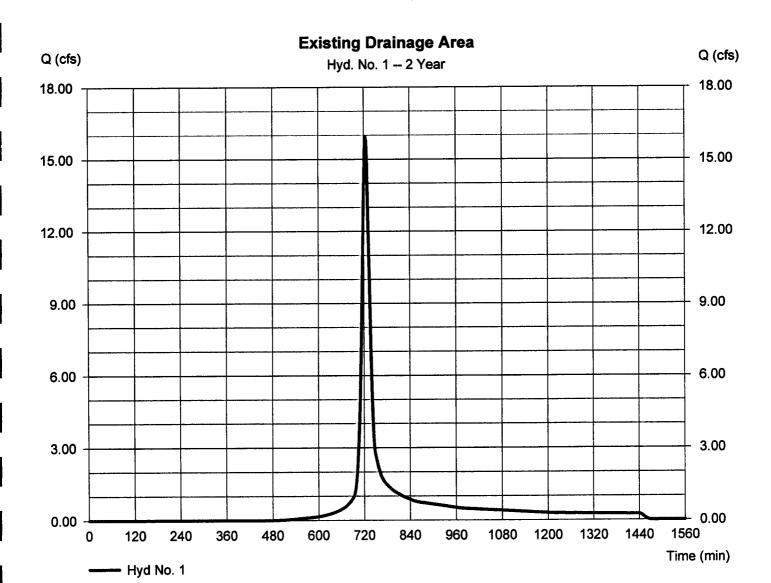
Shape factor

Hyd. No. 1

Storm duration

Existing Drainage Area

Peak discharge = 15.93 cfs= SCS Runoff Hydrograph type = 724 min Time to peak Storm frequency = 2 yrs= 49,857 cuft= 2 min Hyd. volume Time interval = 83 Curve number = 7.390 acDrainage area Hydraulic length = 0 ft= 0.0 % Basin Slope Time of conc. (Tc) $= 18.00 \, \text{min}$ Tc method Distribution = Type II Total precip. = 3.50 in



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

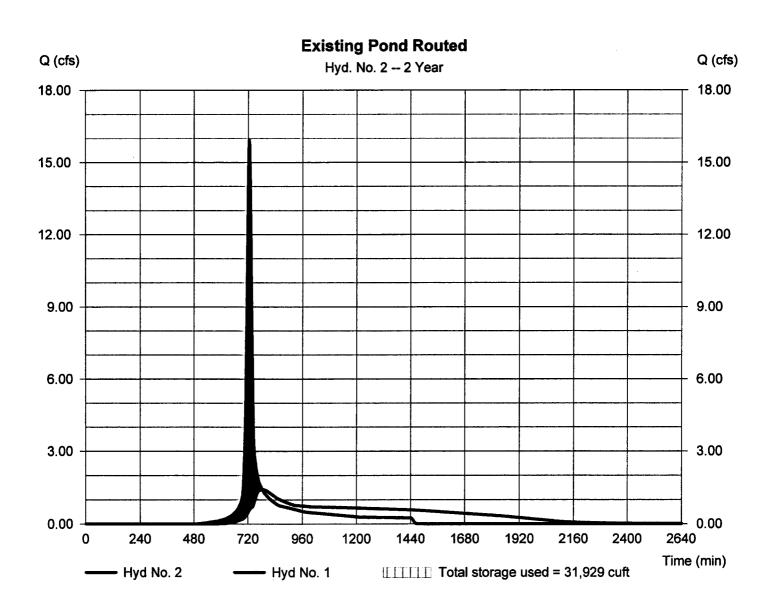
Monday, 00 17, 2013

Hyd. No. 2

Existing Pond Routed

Hydrograph type = Reservoir Peak discharge = 1.425 cfsStorm frequency = 2 yrsTime to peak = 782 min Time interval = 2 min Hyd. volume = 49,820 cuft= 1 - Existing Drainage Area Max. Elevation Inflow hyd. No. $= 85.48 \, \mathrm{ft}$ Reservoir name = Existing Pond Max. Storage = 31,929 cuft

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

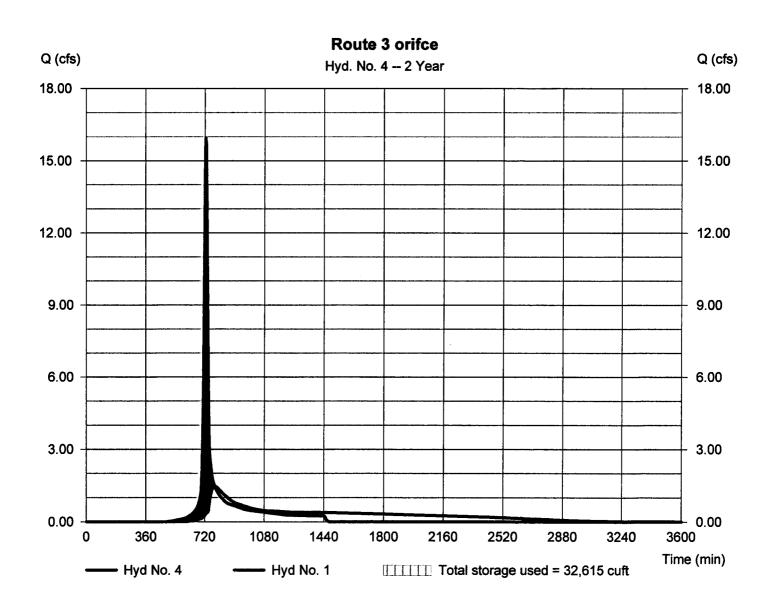
Monday, 00 17, 2013

Hyd. No. 4

Route 3 orifce

Hydrograph type = Reservoir Peak discharge = 1.451 cfsStorm frequency Time to peak = 2 yrs= 780 min Time interval Hyd. volume = 2 min = 49,813 cuft Inflow hyd. No. Max. Elevation = 1 - Existing Drainage Area $= 85.55 \, \mathrm{ft}$ Reservoir name = 3 orifice Max. Storage = 32,615 cuft

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.



Hydrograph Summary Report
Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	33.23	2	724	104,785			******	Existing Drainage Area
2	Reservoir	15.81	2	738	104,748	1	86.98	48,155	Existing Pond Routed
4	Reservoir	16.47	2	736	104,740	1	87.03	48,824	Route 3 orifce
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				A-Paris					
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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Monday, 00 17, 2013

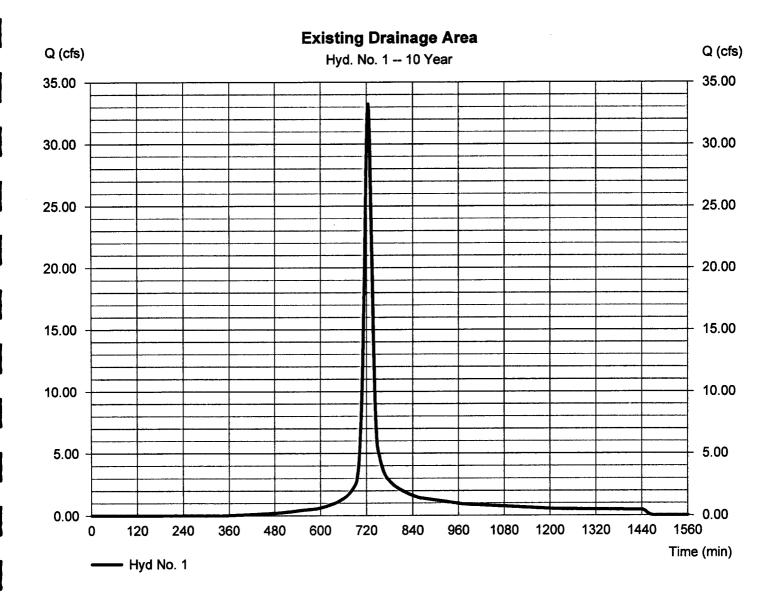
Hyd. No. 1

Existing Drainage Area

= SCS Runoff Peak discharge = 33.23 cfsHydrograph type = 724 min Storm frequency = 10 yrsTime to peak Hyd. volume = 104,785 cuftTime interval = 2 min Curve number = 83 = 7.390 acDrainage area Hydraulic length = 0 ft**Basin Slope** = 0.0 %

Tc method

Time of conc. (Tc) $= 18.00 \, \text{min}$ Distribution = Type II Total precip. = 5.80 in= 484 Shape factor Storm duration = 24 hrs



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

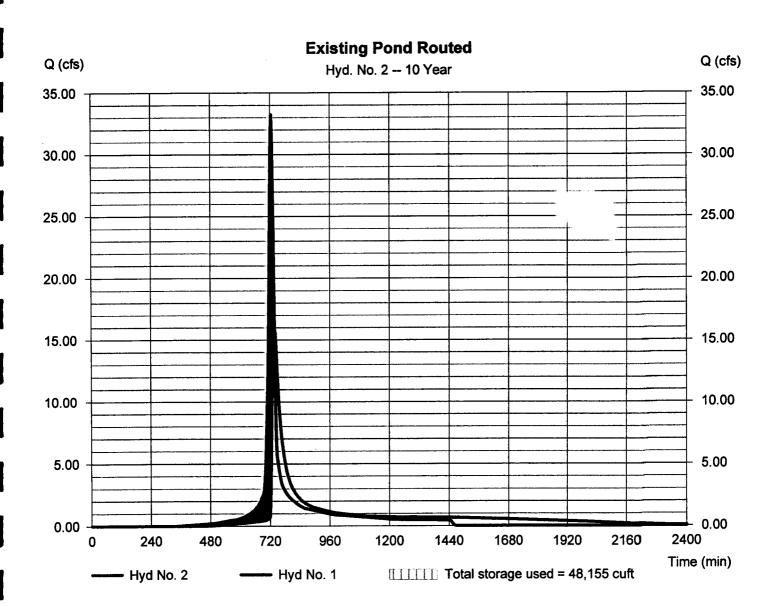
Monday, 00 17, 2013

Hyd. No. 2

Existing Pond Routed

Peak discharge = 15.81 cfs= Reservoir Hydrograph type Time to peak = 738 min = 10 yrs Storm frequency Hyd. volume = 104,748 cuftTime interval = 2 min Max. Elevation = 86.98 ft= 1 - Existing Drainage Area Inflow hyd. No. = 48,155 cuftReservoir name = Existing Pond Max. Storage

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

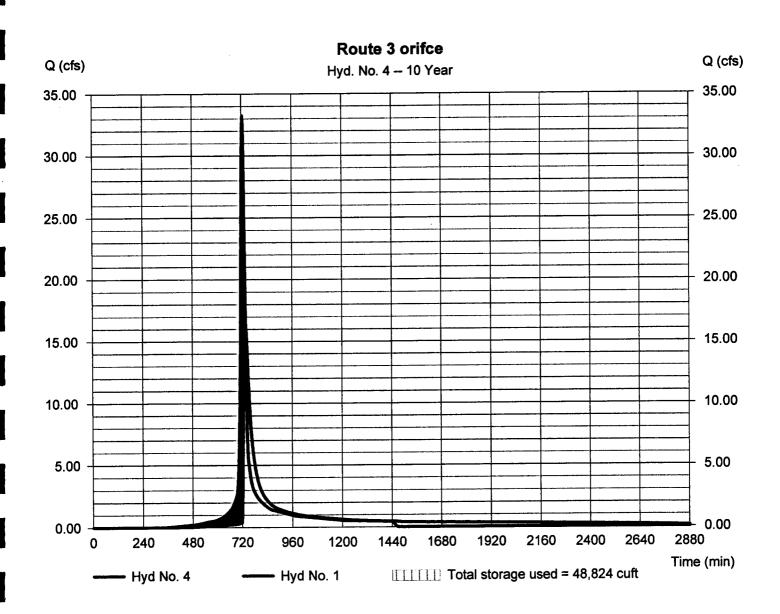
Monday, 00 17, 2013

Hyd. No. 4

Route 3 orifce

= 16.47 cfsPeak discharge Hydrograph type = Reservoir = 736 min Time to peak Storm frequency = 10 yrs= 104,740 cuftHyd. volume Time interval = 2 min Max. Elevation $= 87.03 \, \text{ft}$ = 1 - Existing Drainage Area Inflow hyd. No. = 48,824 cuft Max. Storage Reservoir name = 3 orifice

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.



Hydrograph Summary Report
Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time intervai (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	50.07	2	724	160,348				Existing Drainage Area
2	Reservoir	41.50	2	730	160,312	1	87.58	56,066	Existing Pond Routed
4	Reservoir	42.29	2	730	160,303	1	87.60	56,333	Route 3 orifce
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Monday, 00 17, 2013

Hyd. No. 1

Existing Drainage Area

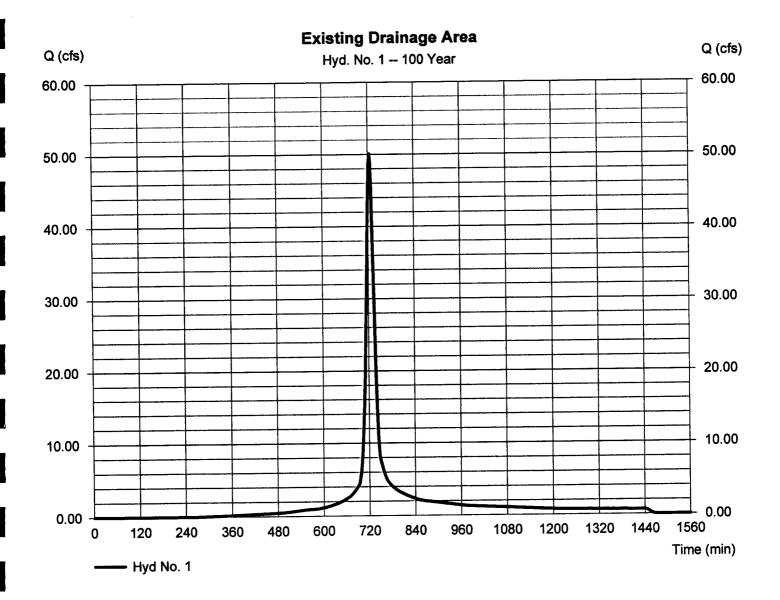
Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Time interval = 2 min
Drainage area = 7.390 ac
Basin Slope = 0.0 %

Tc method

Total precip. = 8.00 in Storm duration = 24 hrs Peak discharge = 50.07 cfs
Time to peak = 724 min
Hyd. volume = 160,348 cuft
Curve number = 83

Curve number = 83
Hydraulic length = 0 ft

Time of conc. (Tc) = 18.00 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

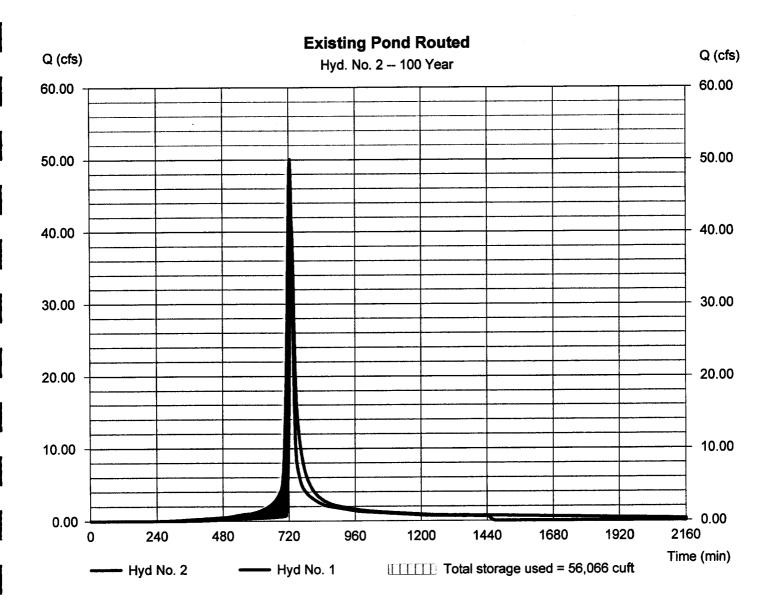
Monday, 00 17, 2013

Hyd. No. 2

Existing Pond Routed

Peak discharge = 41.50 cfs= Reservoir Hydrograph type Time to peak = 730 min = 100 yrsStorm frequency Hyd. volume = 160,312 cuft= 2 min Time interval $= 87.58 \, \mathrm{ft}$ Max. Elevation = 1 - Existing Drainage Area Inflow hyd. No. Max. Storage = 56,066 cuft Reservoir name = Existing Pond

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

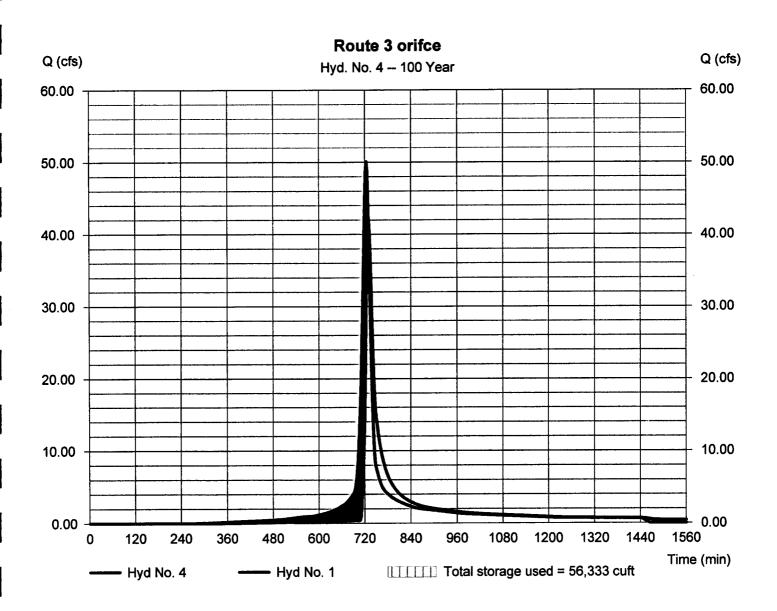
Monday, 00 17, 2013

Hyd. No. 4

Route 3 orifce

Hydrograph type Peak discharge = 42.29 cfs= Reservoir = 730 min Time to peak = 100 yrsStorm frequency Hyd. volume = 160,303 cuftTime interval = 2 min Max. Elevation $= 87.60 \, \text{ft}$ Inflow hyd. No. = 1 - Existing Drainage Area Reservoir name Max. Storage = 56,333 cuft= 3 orifice

Storage Indication method used. Wet pond routing start elevation = 82.20 ft.

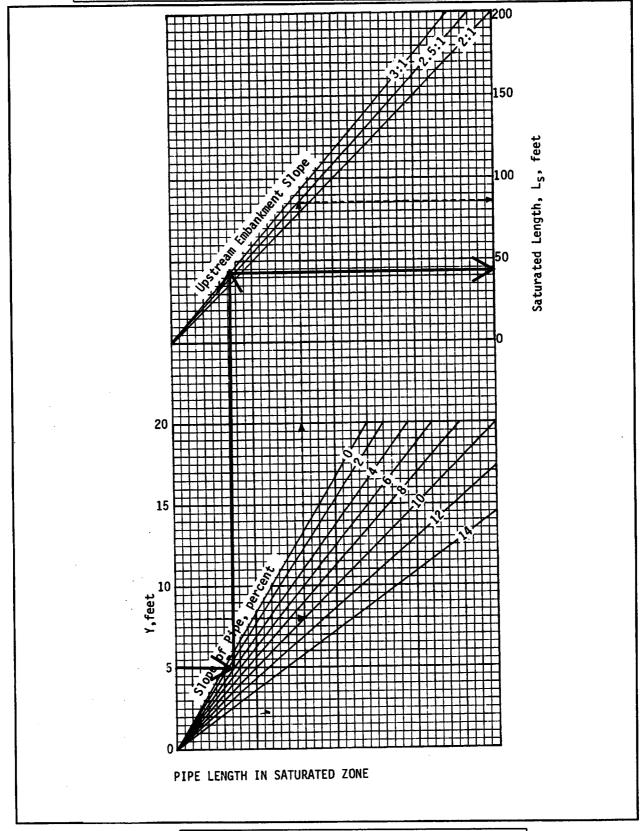


1992

DATE: SEPTEMBER 15, 2011

SUBJECT: ANTI-SEEP COLLAR DESIGN

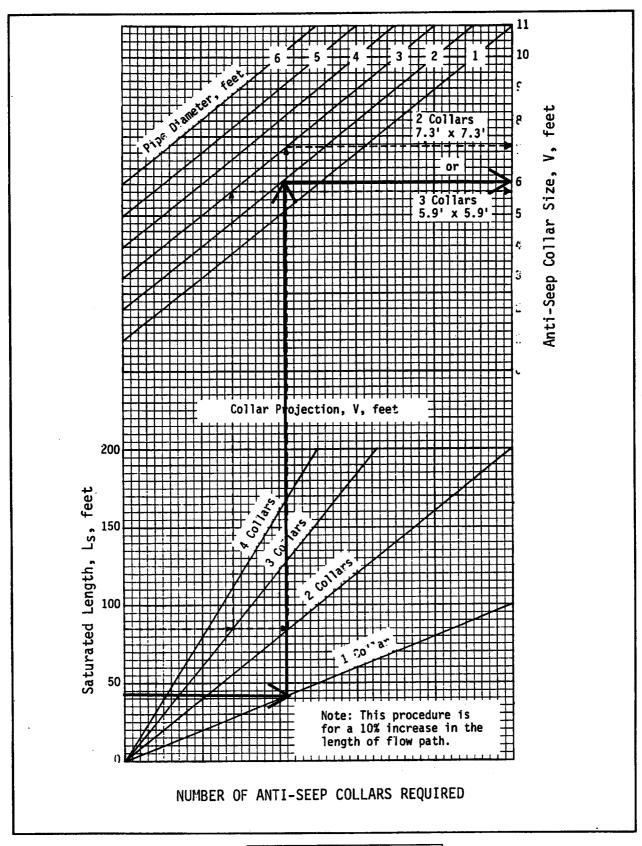
3.14



Source: USDA-SCS

Depth of water at principal spillway crest (Y) = 5 ft. Slope of upstream face of embankment (Z) = 3 :1. 3.79 % Slope of principal spillway barrel (Sb) =

Plate 3.14-11



Source: USDA-SCS

Number of collars required = 1 Dimensions = 6'x6'

Plate 3.14-12



 Project:
 Stonehouse Dam

 Project No.:
 W10119-E-04

 Subject:
 Riprap Basin

 For Circular Culvert

 Date:
 9/24/2012

 Calculated By:
 GVC

Hydraulic Design of Energy Dissipators for Culverts and Channels Hydraulic Engineering Circular No. 14, Third Edition U.S. Department of Transportation Federal Highway Administration - July 2006

Outfall Description:

BMP Outfall

Pipe Diameter (D) or (W_o) =

Flow (Q) =

Tailwater Depth (TW) =

Determine brink depth (y_o):

$$(K_u) \frac{Q}{D^{2.5}} = (1) \frac{40.67}{5.66} = 7.19$$

$$\frac{\text{TW}}{\text{D}} = \frac{1.50}{2.00} = 0.75$$

From Figure 3.4

$$y_o / D$$
 D $y_o = 0.74 \times 2.00$

Determine culvert outlet velocity (V_o) :

$$\frac{\text{TW}}{\text{y}_{0}} = \frac{1.50}{1.48} = 1.014$$

$$A/D^2 = 0.6231$$

From Table B.2 where $y_o / D = d / D$

$$A = A/D^2 x$$

$$D^2 = 0.6231 \times 4.00$$

Determine Froude number (Fr):

$$y_e = (A/2)^{1/2} = 1.12$$

Fr =
$$V_o/[(32.2)(y_e)]^{1/2}$$
 = 2.7

Try $d_{50}/y_e = 0.45$ $d_{50} = 0.45$ x 1.12 = 0.50 FT. or 6.0 IN.

Tailwater Parameter, C_o Equation 10.2 $TW/y_e = 1.50 \div 1.12 = 1.34$ $TW/y_e < 0.75 \qquad C_o = 1.4$ $0.75 < TW/y_e < 1.0 \qquad C_o = 4.0 (TW/y_e) - 1.6$ = 4.0 (1.34) - 1.6 = 3.77 $1.0 < TW/y_e \qquad C_o = 2.4$

 $h_s/y_e = 0.86 (d_{50}/y_e)^{-0.55} (Fr) - C_o Equation 10.1$ $h_s/y_e = 0.86 (0.45)^{-0.55} (2.72) - 2.40$ $h_s/y_e = 1.2313$ $h_s = 1.2313 x 1.12 = 1.37 FT.$ Check

hs / d₅₀ = 2.74 ≥ 2 OK d₅₀ / y_e = 0.45 ≥ 0.1 OK

Riprap Basin Size

Length of Dissipator Pool

 $L_s = 10 \times h_s = 13.7 \text{ FT.}$ or $L_s = 3 \times W_o = 6.0 \text{ FT.}$ Use Larger Value $L_s = 13.7 \text{ FT.}$

Total Length

 $L_{\rm B} = 15 \times h_{\rm s} = 20.6 \ {\rm FT}.$ or $L_{\rm B} = 4 \times W_{\rm o} = 8.0 \ {\rm FT}.$ Use Larger Value $L_{\rm B} = 20.6 \ {\rm FT}.$

Width of Apron

 $W_B = W_o + 2(L_B/3) = 15.7$ FT.

Length of Apron

 L_A = L_B - L_S = 20.6 - 13.7 = 6.9 FT.

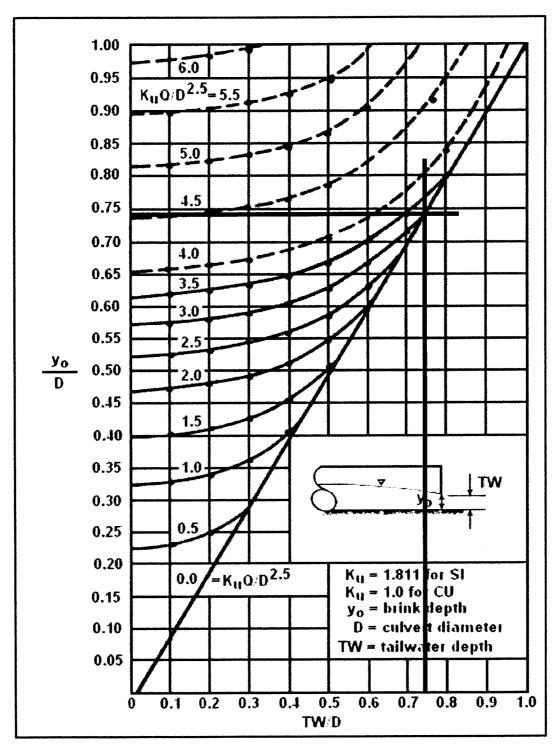


Figure 3.4. Dimensionless Rating Curves for the Outlets of Circular Culverts on Horizontal and Mild Slopes (Simons, 1970)

Table B.2. Uniform Flow in Circular Sections Flowing Partly Full

			(aQn)	(aQn)				(aQn)	(aQn)
y/D	A/D ²	R/D	(D ^{5/3} S ^{1/2})	$(y^{2/3} S^{1/2})$	y/D	A/D ²	R/D	(D ^{8/3} S ^{1/2})	$(g^{(0)})$ $(y^{(0)} S^{(1)2})$
0.01	0.0013	0.0066	0.00007	15.04	0.51	0.4027	0.2531	0.239	1.442
0.02	0.0037	0.0132	0.00031	10.57	0.52	0.4127	0.2562	0.247	0.415
0.03	0.0069	0.0197	0.00074	8.56	0.53	0.4227	0.2592	0.255	1.388
0.04	0.0105	0.0262	0.00138	7.38	0.54	0.4327	0.2621	0.263	1.362
0.05	0.0147	0.0325	0.00222	6.55	0.55	0.4426	0.2649	0.271	1.336
0.06	0.0192	0.0389	0.00328	5.95	0.56	0.4526	0.2676	0.279	1.311
0.07	0.0294	0.0451	0.00455	5.47	0.57	0.1626	0.2703	0.287	1 286
0.08	0.0350	0.0513	0.00604	5.09	0.58	0.4724	0.2728	0.295	1.262
0.09	0.0378	0.0575	0.00775	4.76	0.59	0.4822	0.2753	0.303	1.238
			0.000-		1000	0.4000	0.0770	0.214	1 2 1 5
0.10	0.0409	0.0635	0.0097	4.49	0.60	0.4920	0.2776	0.311	1.215
0.11	0.0470	0.0695	0.0118	4.25	0.61	0.5018	0.2799	0.319	1.192
0.12	0.0534	0.0755	0.0142	4.04	0.62	0.5115	0.2821	0.327	1.170
0.13	0.0600	0.0813	0.0167	3.86	0.63	0.5212	0.2842	0.335	1.148
0.14	0.0668	0.0871	0.0195	3.69	0.64	0.5308	0.2862	0.343	1,126
	0.0700	0.0000	0.0005	254	1000	O E ADE	0.2988	0.350	1,105
0.15	0.0739	0.0929	0.0225	3.54	0.65	0.5405 0.5499	0.2988	0.350	1.103
0.16	0.0811	0.0985	0.0257	3.41	0.66	0.5499	0.2900	0.356	1.064
0.17	0.0885	0.1042	0.0291	3.28 3.17	0.67	0.5594	0.2917	0.366	1.044
0.18	0.0961	0.1097	0.0327	3.17	0.69	0.5780	0.2933	0.380	1.024
0.19	0.0139	0.1152	0.0365	3.00	0.09	0.3790	0.2340	0.300	1.029
0.00	0.4440	0.4206	0.0406	2.96	0.70	0.5872	0.2962	0.388	1.004
0.20	0.1118	0.1206 0.1259	0.0406	2.87	0.71	0.5964	0.2975	0.395	0.985
0.21			0.0448	2.79	0.73	0.6054	0.2987	0.402	0.965
0.22	0.1281 0.1365	0.1312	0.0492	2.79	0.72	0.6143	0.2998	0.409	0.947
0.23	0.1303	0.1304	0.0585	2.63	0.74	0.6231	0.3008	0.416	0.928
0.24	0.1448	0.1410	0,0000	2.00	V.7.4	0.02.0.1	0,0000	0.410	V.VA.V
0.25	0 1535	0.1466	0.0634	2.56	0.75	0.6319	0.3042	0.422	0.910
0.26	0.1623	0.1516	0.0686	2.49	0.76	0.6405	0.3043	0.429	0.891
0.27	0.1711	0.1566	0.0739	2.42	0.77	0.6489	0.3043	0.435	0.873
0.28	0.1800	0.1614	0.0793	2.36	0.78	0.6573	0.3041	0.441	0.856
0.29	0.1890	0.1662	0.0849	2.30	0.79	0.6655	0.3039	0.447	0.838
0.30	0.1982	0.1709	0.0907	2.25	0.80	0.6736	0.3042	0.453	0.821
0.31	0.2074	0.1756	0.0966	2.20	0.81	0.6815	0.3043	0.458	0.804
0.32	0.2167	0.1802	0.1027	2.14	0.82	0.6893	0.3043	0.463	0.787
0.33	0.2260	0.1847	0.1089	2.09	0.83	0.6969	0.3041	0.468	0,770
0.34	0.2355	0.1891	0.1153	2.05	0.84	0.7043	0.3038	0.473	0.753
0.35	0.2450	0.1935	0.1218	2.00	0.85	0.7115	0.3033	0.453	0.736
0.36	0.2546	0.1978	0.1284	1.958	0.86	0.7186	0.3026	0.458	0.720
0.37	0 2642	0.2020	0.1351	1.915	0.87	0.7254	0.3018	0.485	0.703
0.38	0.2739	0.2062	0.1420	1.875	0.88	0.7320	0.3007	0.488	0.687
0.39	0.2836	0.2102	0.1490	1.835	0.89	0.7384	0.2995	0.491	0.670
0.40	0.2934	0.2142	0.1561	1.797	0.90	0.7445	0.2980	0.494	0.654
0.41	0.3032	0.2182	0.1633	1.760	0.91	0.7504	0.2963	0.496	0.637
0.42	0.3130	0.2220	0.1705	1.724	0.92	0.7560	0.2944	0,497	0.621
0 43	0.3229	0.2258	0.1779	1,689	0.93	0.7612	0.2921	0.498	0.604
0.44	0.3328	0.2295	0.1854	1.655	0.94	0.7662	0.2895	0.498	0.588
0.45	0.3428	0.2331	0.1929	1.622	0.95	0.7707	0.2865	0.498	0.571
0.46	0.3527	0.2366	0.201	1.590	0.96	0.7749	0.2829	0.496	0.553
0.47	0.3627	0.2401	0.208	1.559	0.97	0.7785	0.2787	0.494	0.535
0.48	0 3727	0.2435	0.216	1 530	0.98	0.7817	0.2735	0.489	0.517
0.49	0.3827	0.2468	0.224	1.500	0.99	0.7841	0.2666	0.483	0.496
	1		<u> </u>	ļ	_			A	
0.50	0.3927	0.2500	0.232	1,471	1.00	0.7854	0.2500	0.463	0.463
y = dep	oth of flow, n	n (ft)			Q = dise	cnarge by M	ianning's Ed	uation, m³/s	s (π ⁻ /\$)

D = diameter of pipe, m (ft)

A = area of flow, m^2 (ft²)

R= hydraulic radius, m (ft) Source: USBR (1974)

n = Manning's coefficient

S = channel bottom and water surface slope

 α = units conversion = 1.49 for SI, 1 for CU

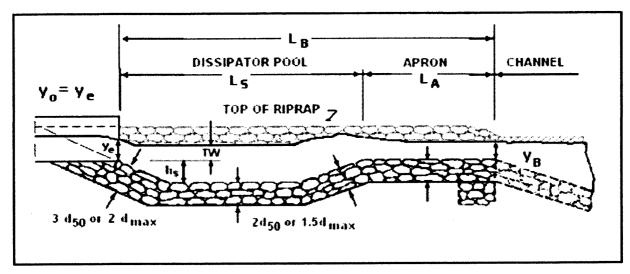


Figure 10.1. Profile of Riprap Basin

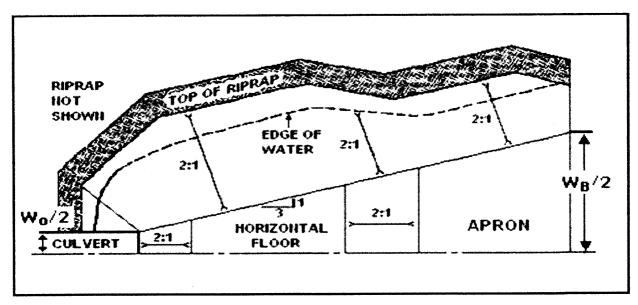


Figure 10.2. Half Plan of Riprap Basin

DRAINAGE CALCULATIONS

Krivisonmente/ Options

FOR

PECEIVED

STONEHOUSE ELEMENTARY

SITE:

James City County

SUBMITTED TO:

Environmental Division James City County

Prepared By:

AES Consulting Engineers 5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188

April 18, 2012

AES Project No. W10119-E-04

W10119-E-94_Stormwater Management Report doc



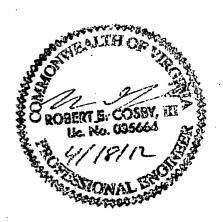




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- -18" Existing Storm System Outlet Protection Design

STORM WATER NARRATIVE

PROJECT DESCRIPTION

This project involves the conversion of an existing dry pond into a constructed wetlands BMP at Stonehouse Elementary.

EXISTING SITE CONDITIONS

The existing site is a dry pond located in the northern corner of the Stonehouse Elementary School property.

ADJACENT PROPERTIES

The project is bordered on the northeast and northwest by wooded areas, on the southwest by grass field, and on the south by the school parking lot.

SOILS

The project area consists of 11C-Craven-Uchee complex and 19B Kempsville-Emporia Fine Sandy Loam with slopes ranging from 2 to 50 percent.

CRITICAL EROSION AREAS

There are areas of 25% slope impacts in this project. These amount to 0.166 acres or 25.9% of the total disturbed area.

STORMWATER MANAGEMENT & WATER QUALITY

Stormwater Management and water quality will be attained for this project through the use of the proposed Constructed Wetlands. The constructed wetlands consist of forebays at the locations of incoming pipes, deep pools that will remain wet, and the normal pool volume. Sizing of the facility is based on the Treatment Volume of 12,894 cubic feet. Of this volume, deep pool should provide 25% (3,224 cubic feet) and the normal pool should provide 50% (6,447 cubic feet). According to the Virginia DCR Stormwater Design Specification No. 13, deep pools consist of the deep wet pool, micropool, and forebay areas.

The proposed wetlands will provide 11,538 cubic feet of total treatment volume. The deep pools have a volume of 3,165 cubic feet. The normal pool includes the volume provided under elevation 83.22 which totals 5,120 cubic feet.

The channel protection volume required for the drainage area to the pond is 20,720 cubic feet. The channel protection volume provided is 24,609 cubic feet at the riser elevation of 85.26. An emergency spillway is provided at elevation 87.00 which will be utilized during 100-year storm events.

Rip-rap outlet protection is provided at both the outfalls of the incoming pipes in the proposed wetlands. It is also provided at the outfall of the proposed storm system.

RESULTS & CONCLUSIONS

Due to the constraints of the existing pond design full compliance with the DCR technical specifications for a constructed wetlands can not be achieved. Specifically the 1 year Channel Protection Volume is provided, but at a depth greater than the 1 foot recommended. All other requirements regarding volume to be provided in the wet pool and extended detention volume are provided. Based on this analysis the new facility will have a higher pollutant removal efficiency as a constructed wetlands than the existing dry extended detention facility located on site. Therefore this facility as designed will improve the water quality benefits from the site, and maintain the water quantity controls consistent with the original facility.

Stonehouse Elementary School Dam CALCULATION FOR SCS HYDROGRAPH GENERATION AND CHANNEL PROTECTION **FOR Existing Pond** Project No. W10119-E-04 25-Feb-11

PRE-DEVELOPMENT CONDITIONS TO POINT OF CONCERN

69

Pre-Development Drainage Area to Point of Concern =
 Pre-development Land Use, Soil Classification and Calculation of Composite Curve Number

7.39 Acres

18 minutes

-		Soil Type	Soil Hydrologic Group	Pre-Development Land Use	Area of Land Use (in Acres)	Curve Number for Land Use (CN)	Adjusted (CN)
	1)	Composite B/C Soils	С	Open Space (Good)	4.59	74	340
	2)	Impervious Cover	N/A	Impervious Cover	2.8	98	274
	3)					. 0	0
	4)					0	0
	5)					0	Ö
	6) 7)					ŏ	Ö.
		Totals =			7.39		614
		Composite CN =					83
C.	1)	-Development Time of Concentration Overland Flow (maximum 300 fer Surface description (table 5-7) Manning's roughness coefficient, Length of overland flow, L 2-year 24-hour rainfall, P2 Average slope of overland flow, Travel time, Tt = (0.007*(n*L)*0.8	et) , n (table 5-7) s s)/(P2^0.5*s^0.4)				Dense grasses 0.24 50 Feet 3.6 inches 0.03 feet per foot 0.11 hours
•	2)	Shallow concentrated flow (maxin Surface description, paved or unj Length of shallow concentrated fl Average slope of shallow concent Average velocity, v Travel time, Tt = L/(3600°v)	oaved ow, L				unpaved 300 Feet 0.02 feet per foot 1.0 feet per second 0.08 hours
39	3)	Channel or Pipe Flow Length of channel flow, L Average velocity of channel flow, Travel time, Tt = L/(3600°v)	v				550 Feet 1.5 feet per second 0.10 hours
		Total Time of Concentration =					0.29 hours



Project:	Stonehouse Dam
Project No.:	W10119-04
Subject:	1 yr-24 hr Drawdown Calculation
	Kerplunk Method
Date:	3/9/2012 (Revised: 4/9/2012)
Calculated By:	GVC
	3/9/2012 (Revised: 4/9/2012)

Channel Protection Volume:

Drainage Area

7.39 Acres

Runoff Curve No.

83

1-Yr, 24-Hr Storm Volume

2.8 Inches

Direct Runoff

(From TR55 Equations 2-3 & 2-4)

Q=

1.29 inches

Channel Protection Volume = DA x Q x 60%

(Virginia Stormwater Managment Handbook section 5-6.2 - Method 2)

5.71 Ac-in

20,720 cubic feet

Determine Volume of Pond by Contour (starting at invert of low flow orifice):

Elevation	Incremental Depth	Area (sq. ft.)	Volume (cu. ft.)	Volume (cu. yd.)	Sum Volume (cu. ft.)	Sum Volume (cu. yd.)	Incremental Avg Head ¹ (feet)	incremental Avg Flow ¹ (feet)	Incremental Drawdown Time ¹ (hrs)
_78.7	0.0	304	-	-	-	<u>-</u>			
79.7	1.0	719	512	19	512	19	0.50	0.24	0.59
80.7	1.0	1,235	977	36	1,489	55	1.50	0.49	0.56
81.7	1.0	1,851	1,543	57	3,032	112	2.50	0.64	0.67
82.0	0.3	4,209	848	31	3,880	144	3.14	0.72	0.33
83.0	1.0	7,787	5,998	222	9,878	366	3.78	0.80	2.09
84.0	1.0	8,684	8,236	305	18,113	671	4.78	0.90	2.53
85.0	1.0	9,617	9,151	339	27,264	1,010	5.42	0.96	0.75
86.0	1.0	10,595	10,106	374	37,370	1,384	0.00	0.00	0.00
87.0	1.0	11,973	11,284	418	48,654	1,802	0.00	0.00	0.00
88.0	1.0	14,395	13,184	488	61,838	2,290	0.00	0.00	0.00
		Total	61,838	2,290					4.22

¹ Incremental values computed from Channel Protection Volume Elevation

Elevation of Low Flow Orifice Invert 82.22 feet 84.28 feet Elevation of 1-yr, 24-hr Storage Volume 4.00 inches Size of Orifice 4.22 hrs

Total Average Drawdown Time

NOTE: MAINTAINING EXISTING LOW FLOW ORIFICE SIZE

W10119-E-04_Existing Pond and Proposed Wetlands.gpw

Hydraflow Table of Contents

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

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Hydrograph Summary Report
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

yd. o.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	10.95	2	724	34,533				Existing Drainage Area
2	Reservoir	0.579	2	852	30,184	1	84.29	20,597	Existing Pond Routed
									İ
 N1	0119-E-04_l	Existina F	ond and	l Propose	d Riettland	Regions 1 Y	'ear	Thursday	00 15, 2012

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

Hyd. No. 1

Existing Drainage Area

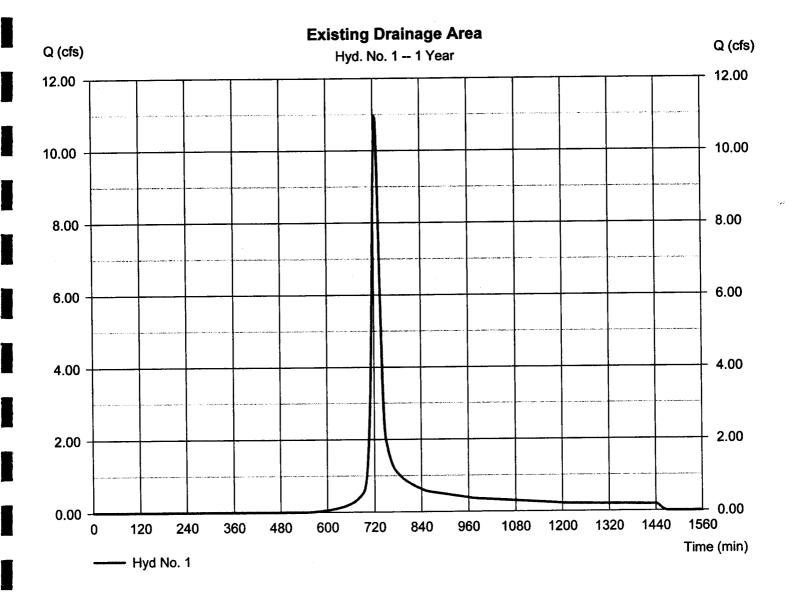
Hydrograph type = SCS Runoff
Storm frequency = 1 yrs
Time interval = 2 min
Drainage area = 7.390 ac
Basin Slope = 0.0 %
Tc method =

Total precip. = 2.80 in
Storm duration = 24 hrs

Peak discharge = 10.95 cfs
Time to peak = 724 min
Hyd. volume = 34,533 cuft

Curve number = 83 Hydraulic length = 0 ft

Time of conc. (Tc) = 18.00 min
Distribution = Type II
Shape factor = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

Hyd. No. 2

Inflow hyd. No.

Reservoir name

Existing Pond Routed

Hydrograph type Storm frequency Time interval

= 1 yrs = 2 min

= Reservoir

1 - Existing Drainage AreaExisting Pond

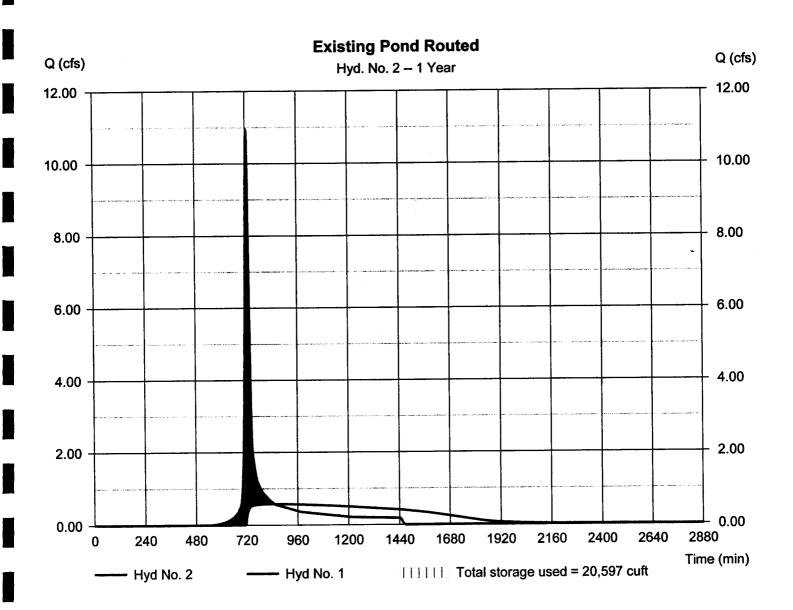
Peak discharge

= 0.579 cfs

Time to peak = 852 min Hyd. volume = 30,184 cuft

Max. Elevation = 84.29 ft Max. Storage = 20,597 cuft

Storage Indication method used. Wet pond routing start elevation = 79.92 ft.



Pond Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

Pond No. 1 - Existing Pond

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 78.72 ft

Stage / Storage Table

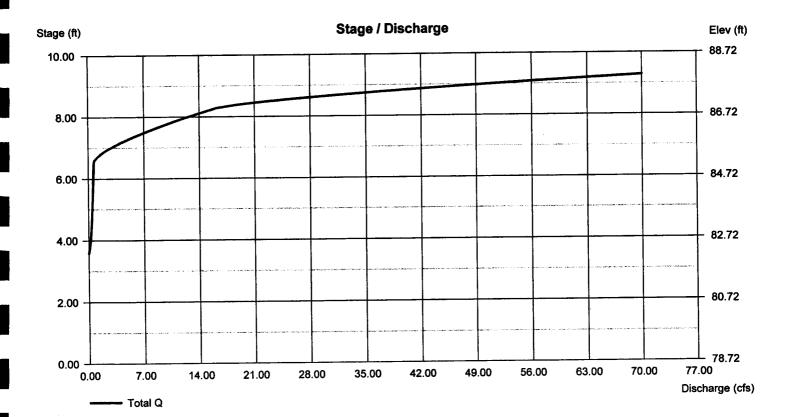
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	78.72	304	0	0
1.00	79.72	719	497	497
2.00	80.72	1,235	965	1,462
3.00	81.72	1,851	1,532	2,995
3.28	82.00	4,209	826	3,821
4.28	83.00	7,787	5,906	9,727
5.28	84.00	8,684	8,231	17,958
6.28	85.00	9,617	9,146	27,103
7.28	86.00	10,595	10,101	37,204
8.28	87.00	11,973	11,276	48,480
9.28	88.00	14,395	13,164	61, 644

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	4.00	0.00	0.00	Crest Len (ft)	= 2.00	15.00	0.00	0.00
Span (in)	= 24.00	4.00	0.00	0.00	Crest El. (ft)	= 85.26	87.00	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	2.60	3.33	3.33
invert El. (ft)	= 79.06	82.22	0.00	0.00	Weir Type	= Rect	Broad		
Length (ft)	= 49.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 3.63	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (b	y Contour)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydrograph Summary Report
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1 2	SCS Runoff Reservoir	15.93 0.901	2	724 834	49,857 45,508	1	85.34	30,564	Existing Drainage Area Existing Pond Routed
								71.	00.45, 2040
W	10119-E-04 __	_Existing	rond an	a Propos	ea waataan	arsegpwor. 2 \	ear	i nursday,	00 15, 2012

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

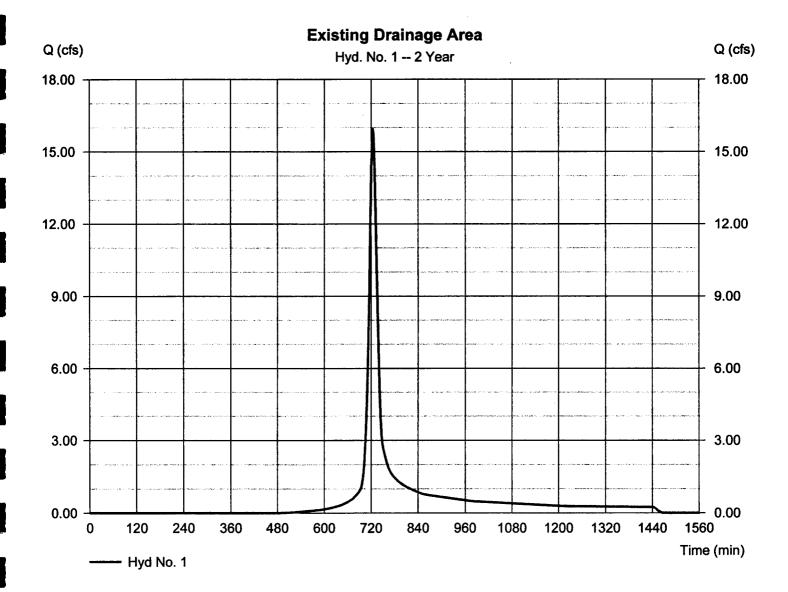
Hyd. No. 1

Existing Drainage Area

Peak discharge Hydrograph type = SCS Runoff = 15.93 cfsStorm frequency = 2 yrsTime to peak $= 724 \, \text{min}$ Time interval = 2 min Hyd. volume = 49,857 cuftCurve number = 7.390 ac= 83 Drainage area Hydraulic length **Basin Slope** = 0.0 % = 0 ftTime of conc. (Tc) $= 18.00 \, \text{min}$

Tc method

Distribution Total precip. = 3.50 in= Type II = 484 Shape factor Storm duration = 24 hrs



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

Hyd. No. 2

Existing Pond Routed

Hydrograph type Storm frequency Time interval

= Reservoir = 2 yrs

Peak discharge Time to peak Hyd. volume

= 0.901 cfs= 834 min = 45,508 cuft

Inflow hyd. No.

= 2 min = 1 - Existing Drainage Area

Max. Elevation

 $= 85.34 \, \mathrm{ft}$

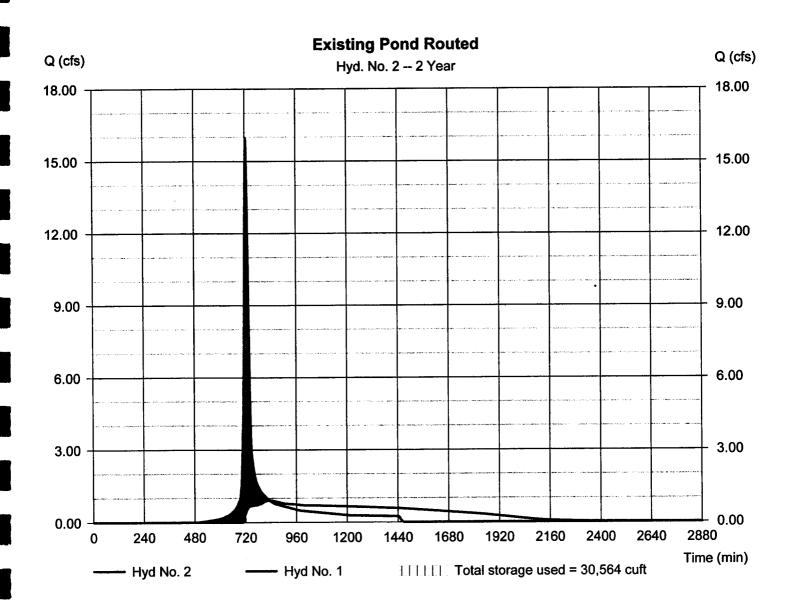
Reservoir name

= Existing Pond

Max. Storage

= 30,564 cuft

Storage Indication method used. Wet pond routing start elevation = 79.92 ft.



Hydrograph Summary Report
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	33.23	2	724	104,785				Existing Drainage Area
2	Reservoir	14.80	2	738	100,436	1	86.89	47,280	Existing Pond Routed
			i.						
							:		
W	/10119-E-04 ₋	Existing	Pond ar	nd Propos	ed Westiaan	dPsegipvolr. 1	0 Year	Thursday	, 00 15, 2012

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

Hyd. No. 1

Existing Drainage Area

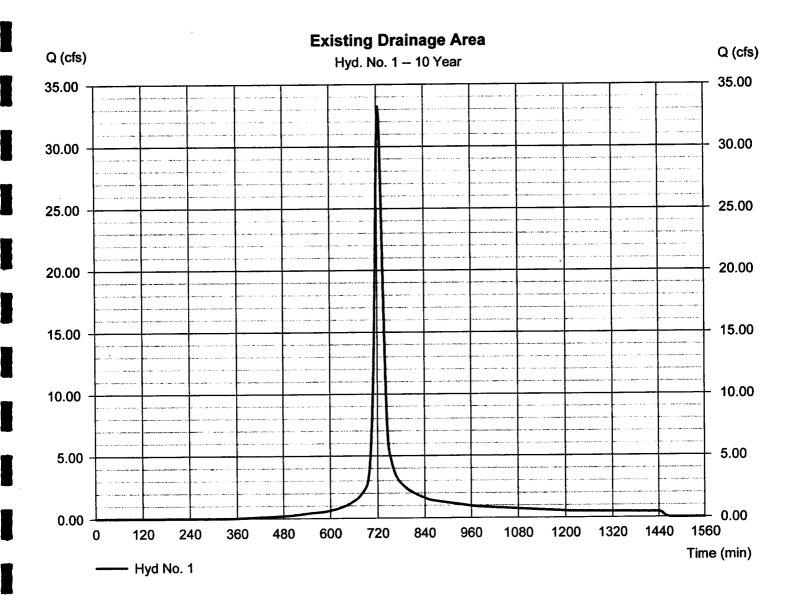
= SCS Runoff Hydrograph type Storm frequency = 10 yrs= 2 min Time interval = 7.390 acDrainage area = 0.0 %**Basin Slope**

Tc method

= 5.80 inTotal precip. = 24 hrs Storm duration

= 33.23 cfsPeak discharge Time to peak = 724 min = 104,785 cuftHyd. volume = 83 Curve number = 0 ftHydraulic length

 $= 18.00 \, \text{min}$ Time of conc. (Tc) Distribution = Type II = 484 Shape factor



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

Hyd. No. 2

Existing Pond Routed

Hydrograph type = Reservoir Storm frequency = 10 yrs Time interval = 2 min

Inflow hyd. No. Reservoir name = 2 min = 1 - Existing Drainage Area

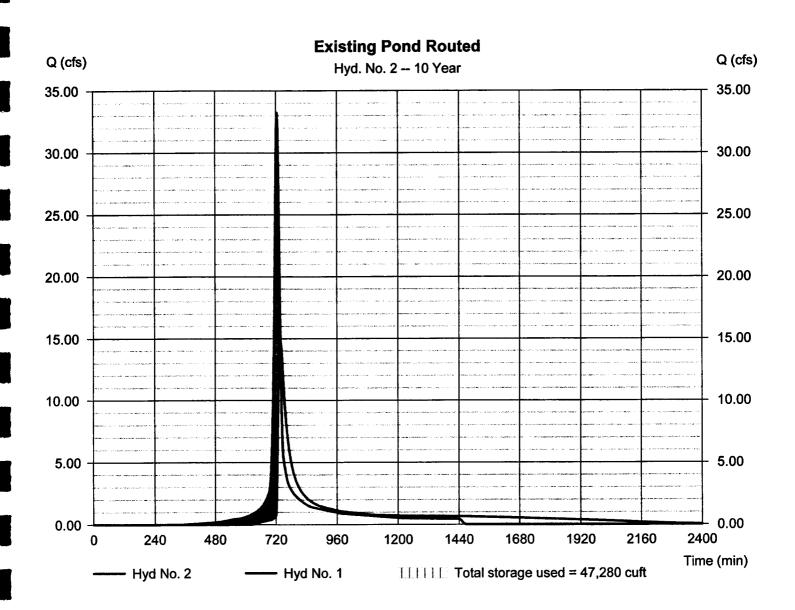
= Existing Pond

Peak discharge Time to peak = 14.80 cfs = 738 min

Hyd. volume = 100,436 cuft
Max. Elevation = 86.89 ft

Max. Storage = 47,280 cuft

Storage Indication method used. Wet pond routing start elevation = 79.92 ft.



Hydrograph Summary Report
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Hyd. No.	Hydrograph type (origin)	flow	interval	Peak	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	50.07	2	724	160,348				Existing Drainage Area
2	Reservoir	40.67	2	730	155,999	1	87.56	55,877	Existing Pond Routed
!									
									·
			:						
			:						
				i					
						:			
W1	0119-E-04_I	Existing F	ond and	d Propose	d Rettend	Regipel: 100) Year	Thursday,	00 15, 2012

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

Hyd. No. 1

Existing Drainage Area

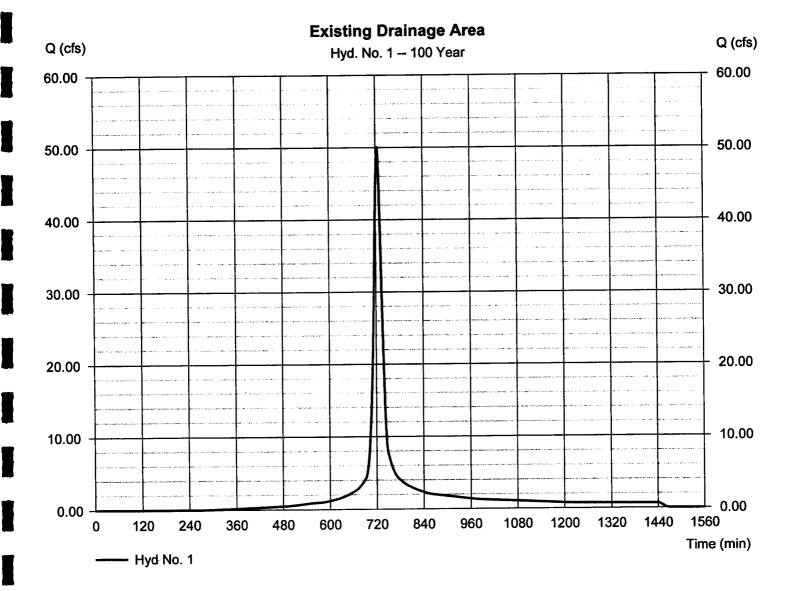
= SCS Runoff Hydrograph type = 100 yrsStorm frequency = 2 min Time interval = 7.390 acDrainage area **Basin Slope** = 0.0 % Tc method

Total precip. = 8.00 inStorm duration = 24 hrs

= 50.07 cfsPeak discharge Time to peak = 724 min = 160,348 cuft Hyd. volume

Curve number = 83 Hydraulic length = 0 ft

Time of conc. (Tc) $= 18.00 \, \text{min}$ = Type II Distribution Shape factor = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc. v9

Thursday, 00 15, 2012

= 40.67 cfs

 $= 730 \, \text{min}$

Hyd. No. 2

Existing Pond Routed

Hydrograph type Storm frequency = Reservoir

= 100 yrs

= 1 - Existing Drainage Area

Inflow hyd. No. Reservoir name

Time interval

= 2 min

= Existing Pond

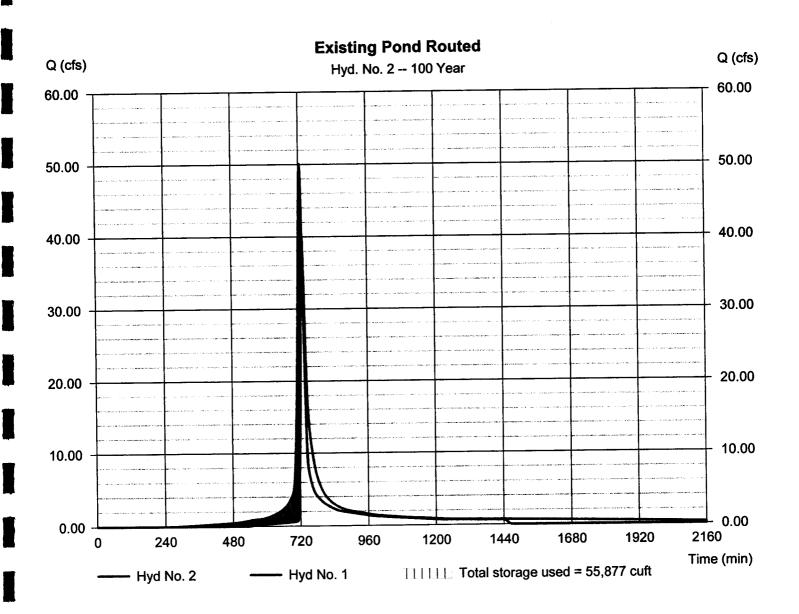
Peak discharge

Time to peak

= 155,999 cuft Hyd. volume $= 87.56 \, \mathrm{ft}$

Max. Elevation = 55,877 cuftMax. Storage

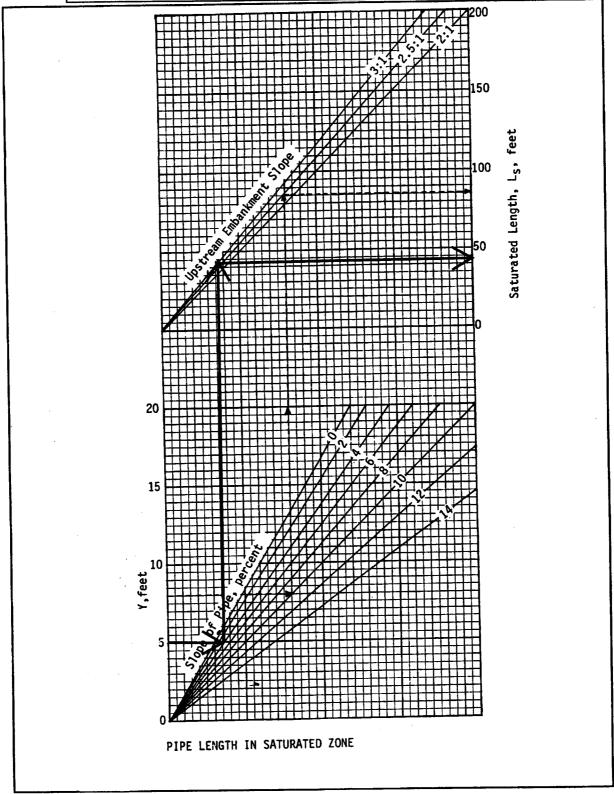
Storage Indication method used. Wet pond routing start elevation = 79.92 ft.



DATE: SEPTEMBER 15, 2011

SUBJECT: ANTI-SEEP COLLAR DESIGN

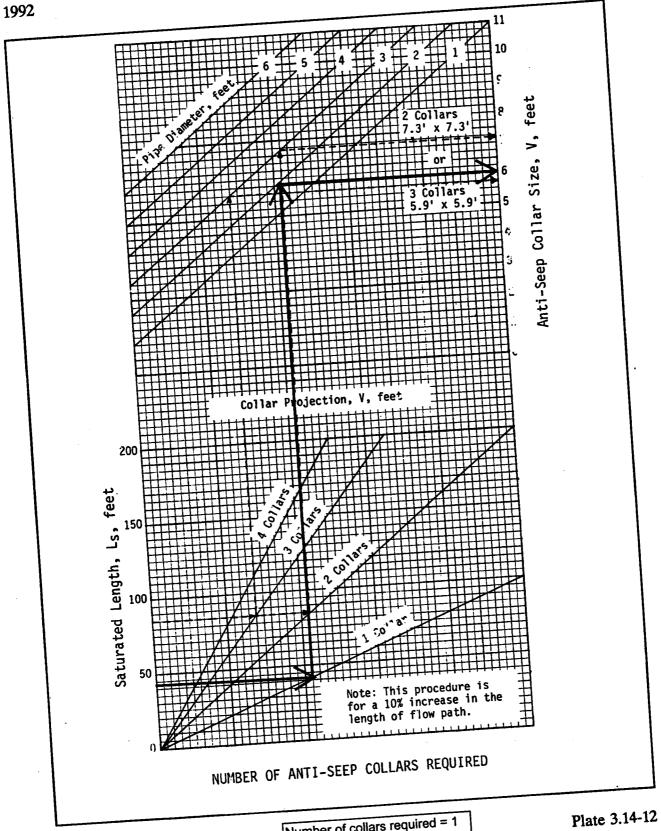




Source: USDA-SCS

Depth of water at principal spillway crest (Y) = Slope of upstream face of embankment (Z) = 3 :1. 3.79 % Slope of principal spillway barrel (Sb) =

Plate 3.14-11



Source: USDA-SCS

Number of collars required = 1 Dimensions = 6'x6'

Storm Sewer Tabulation

	Len	Drng Area	1	Rnoff	Area x C	ပ	2		Rain ()	Total	Cap full	8	Pipe	-	Invert Elev	&	HGL Elev	2	Grnd / Rim Elev	im Elev	Line ID	
Incr Total		<u> </u>			Incr	Total	Inlet	Syst					Size	Slope	5	<u>s</u>	ď	g J	ក្ន	<u>s</u>		
(ft) (ac) (ac)		ă	~	<u></u>			(min)	(min)	(in/hr) (cfs)		(cfs)	(ft/s)	(iii)	(%)	(ft)	Œ	(£)	£)	(tt)	(£t)		
73.000 0.46 0		•	0.57	0.45	0.21	0.27	5.0	5.1	9.3	43.15	52.94	13.78	24	5.48	63.00	67.00	64.97	68.97	63.00	72.00	1-2 TO 1-1	
69.000 0.11 0.		o	0.11	0.55	90.0	90:0	5.0	5.0	9.3	41.23	59.34	13.18	74	6.88	67.00	71.75	68.97	73.71	72.00	75.75	1-3 TO 1-2	
26.000 0.00 0			0.00	0.00	00:00	0.00	0:0	0.1	0.0	24.49	71.52	8.12	24	10.00	71.75	74.35	73.71	76.10	75.75	81.70	1-4 TO 1-3	
39.000 0.00 0.		o	0.00	0.00	0:00	0.00	0.0	0.0	0.0	24.49	43.76	11.05	25	3.74	77.60	79.06	78.67	81.87	81.70	85.26	OS TO 1-4	
Project File: W10119-04_Storm System Calcs.stm	9-04_Stor	١٥	rm Sys	stem Cal	lcs.stm										Number	Number of lines: 4	•		Run Da	Run Date: 4/9/2012	12	ŀ

NOTES:Intensity = 473.32 / (Inlet time + 30.90) ^ 1.10; Return period =Yrs. 100; c = cir e = ellip b = box

Storm Sewers v9.00

Stonehouse Elementary Dam 9/15/2011 (Revised:4/9/2012) **Outlet Protection** W10119-04 300 500 200 Project No.: Subject: Calculated By: ft3/sec. 24 0.8 DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ($T_{\rm w}$ < 0.5 DIAMETER) 50 Discharge ≥ Outlet Location: Storm System Outfall 8 9 Outlet Pipe Diameter, cfs CONSULTING ENGINEERS 43.15 Source: USDA-SCS Plate 3.18-3

III - 164

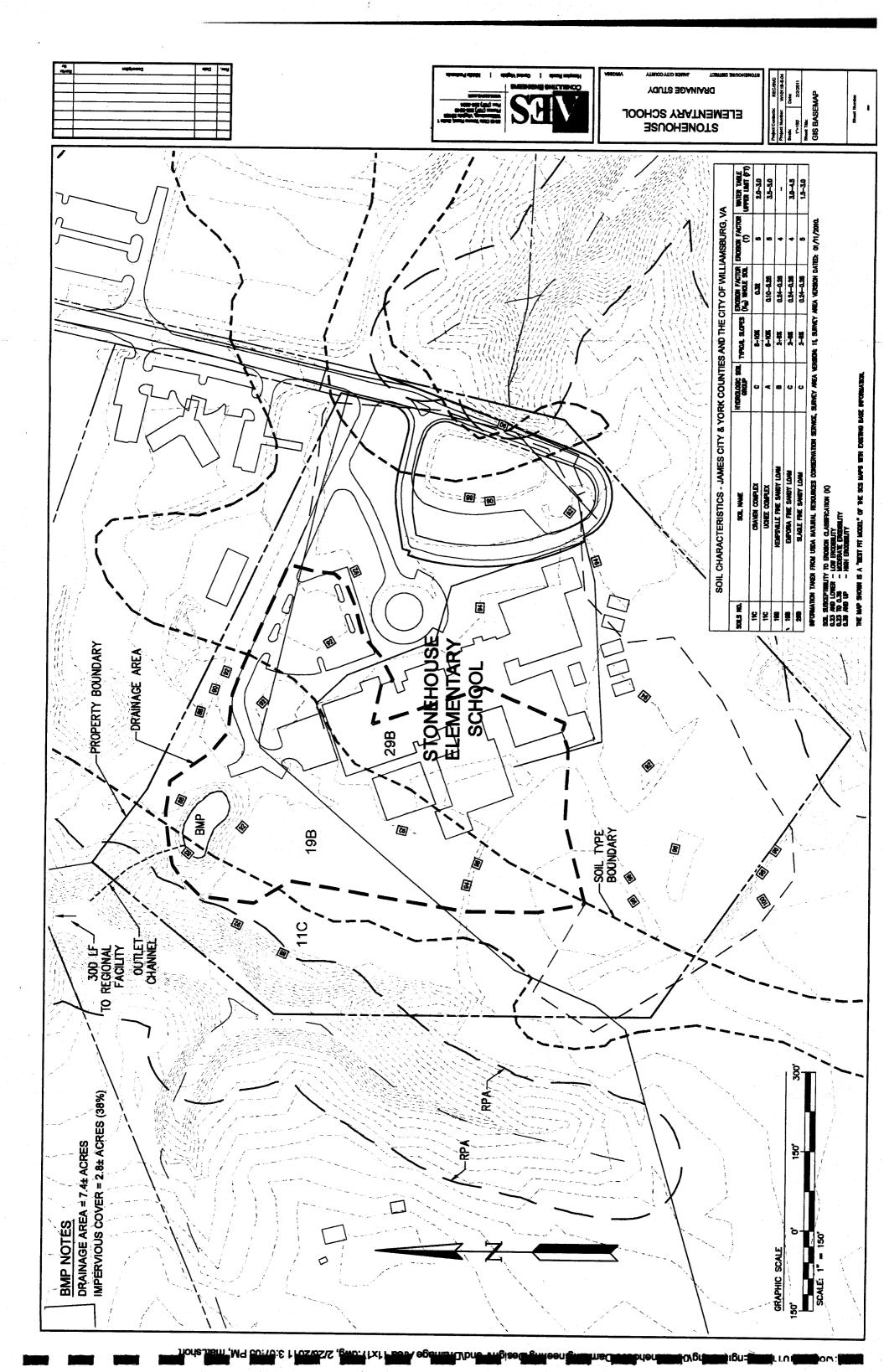
3.18

" " " <u>"</u>

jŝ

d₅₀ Riprap Size, feet

1992

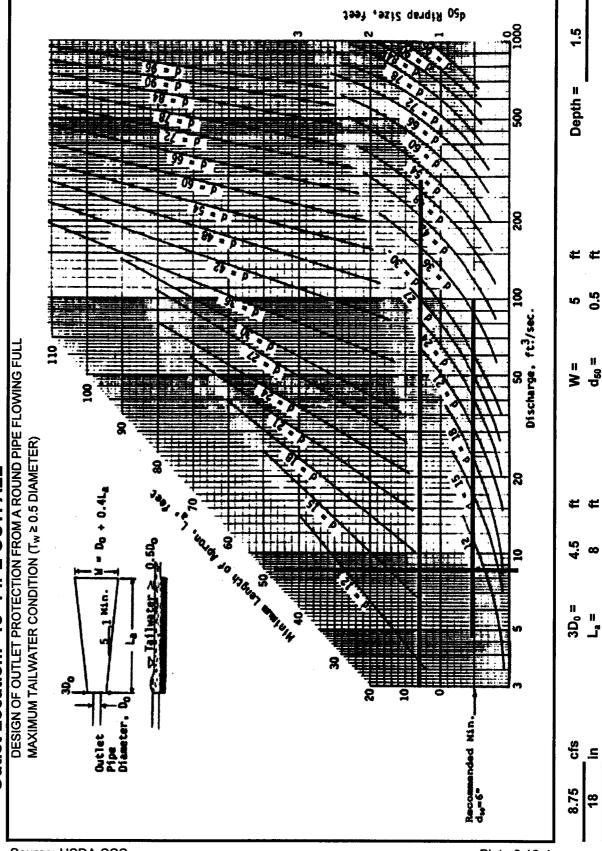


#

Q	NEERS
Z	CONSULTING ENGINEERS
A	CONSU

Stonehouse Dam	W10119-E-04	Outlet Protection	3/10/2012	LRB	
Project:	Project No.:	Subject:	Date:	Calculated By:	

Outlet Location: 18" PIPE OUTFALL



Source: USDA-SCS

Plate 3.18-4

TRANSMITTAL

Chukonmenta/ Oiligio

DATE:

September 27, 2013

SEP 3 0 2013

TO:

Records Management (1 copy)

JCSA (3 copies)

Fire (1 copy)

Engineering and Resource Protection (1 copy)

Virginia Department of Transportation (1 copy)

PECEIVED

FROM:

Jose Ribeiro, Senior Planner

SUBJECT:

SP-0039-2012, Stonehouse Elementary School Stormwater Facility

Retrofit/Repair

TAX ID:

1310100020

ACTION:

For your files.